

## Route 7 Concept Study

Traffic Operations and Safety Report-Draft
February 10, 2021

## EXECUTIVE SUMMARY

This traffic operations and safety report examines existing and projected future conditions along Route 7 in Loudoun County, Virginia, between Dranesville Rd (Route 228) at the Fairfax County line to the Route 28 interchange, a distance of approximately 4.25 miles. This study includes an evaluation of the history of reported crashes occurring during recent years, an analysis of traffic operations along the corridor under existing conditions, travel demand forecasts for a 2040 No-Build alternative and (to-date) one 2040 Build alternative, and an analysis of the traffic operations expected under those alternatives.

Based on the data for the intersection-related crashes, it appears that rear-end collisions have been the predominant crash type. Research has shown that the presence of traffic signals can lead to an increase in the frequency of rear-end crashes, particularly in areas with heavier volumes, so these trends are consistent with Route 7 within the study area.

Traffic analyses for this study were performed using VISSIM. These VISSIM models were calibrated in accordance with the VDOT VISSIM Users Guide and the VDOT Traffic Operations and Safety Analysis Manual, Version 2.0 (TOSAM), which recommend following the calibration process as described in the FHWA Traffic Analysis Toolbox Volume III: Guidelines for Applying Traffic Microsimulation Modeling Software (FHWA-HRT-04-040). Traffic volume data for model calibration and analysis were collected in June 2019 and, therefore, were not impacted by the ongoing COVID-19 pandemic.

Traffic volume projections for 2040 were forecast by examining the Loudoun County Travel Demand Model output as well as historical VDOT traffic volume counts and estimates. Based on this evaluation, Loudoun County DTCI found it acceptable to use a $+1 \%$ annual growth rate (applied exponentially) to adjust Existing traffic counts to Year 2040 levels for analysis in this study.

As part of the Route 7 Concept Study, several potential Build alternatives were developed at the sketch planning level and presented to Loudoun County DTCI staff and representatives from other government and institutional stakeholders during a brainstorming work session in August 2020. Of these potential improvement options, the Modified Superstreet Corridor was selected to be the first of several potential alternatives to be retained for more detailed analysis. This concept is referred to as Alternative 1. The primary feature of this alternative is the elimination of all through and left-turn movements from crossstreets along Route 7 and the diversion of those displaced volumes to U -turn movements at some existing intersections and some new signalized intersections to be built solely for this purpose. However, this alternative also assumes the existing cloverleaf interchange along Route 7 at Cascades Pkwy would be replaced with a tight diamond interchange to eliminate ramp junctions along Route 7, and the intersection of Route 7 and Dranesville Road (in Fairfax County) would be rebuilt as a "Green- T " to support a conservative analysis of Route 7 traffic operations downstream of this existing constraining location.

The analysis performed in this study shows that traffic operations would improve at some locations under Alternative 1 while they worsen at other locations under Alternative 1. However, during the PM peak hour, there would not be much change in LOS for Alternative 1 compared to the No-Build alternative.

In terms of density on the Route 7 roadway segments through the Cascades Parkway interchange, the analysis results show an improvement (i.e., reduction) in the density (vehicles per mile per lane) with the tight diamond interchange (TDI) configuration proposed under Alternative 1. This is likely due to the removal of an on- and off-ramp in each direction along Route 7 and the corresponding elimination of the weaving segment between those ramps.

Examining the corridor end-to-end travel times along Route 7 shows that Alternative 1 would result in a substantial improvement (i.e., reduction) in travel time in the peak direction (eastbound) during the AM
peak hour. The time required to travel the 4.25 -mile study corridor eastbound would be reduced by more than 4 minutes - a $28 \%$ reduction in travel time. For reference, the red light (or red interval) duration of the traffic signals along Route 7 is about 80 seconds; therefore, the travel time savings are roughly equivalent to a driver not having to wait at three traffic signals. However, a comparison of the PM peak hour, peak direction (westbound) travel times shows that Alternative 1 would have no impact. The time required to travel the 4.25 -mile study corridor westbound would remain at 11 minutes for Alternative 1 - the same as under the No-Build alternative.

The addition of 6 new traffic signals along Route 7 to accommodate the movements displaced by Alternative 1's modified superstreet configuration may offset the crash-reducing benefits of eliminating some conflict points at the existing intersections. These existing conflict points would be reduced by prohibiting through and left-turn movements from the cross-streets at the existing signalized intersections along Route 7.

## Conclusion

There are several tangible benefits associated with Alternative 1 that are evident when comparing its performance to that of the No-Build alternative:

- Improved AM peak period travel times for eastbound traffic
- Reduced number of conflict points at existing intersections; potentially reducing the likelihood of crashes at those locations

However, there remain several areas where performance would decrease under Alternative 1, such as LOS for the cross-street approaches and for the proposed U-turn movements. Furthermore, the potential for crash reduction under Alternative 1 may be small.

Additional build alternatives may be developed in the future depending on the outcome of Loudoun County DTCl's review of the Alternative 1 benefits and challenges, including the traffic analysis results in this study.

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## 1. INTRODUCTION

The purpose of this report is to summarize the findings of the traffic operations analysis for Route 7 in Loudoun County, Virginia, extending from just west of Route 228 (Dranesville Road) at the Fairfax County/Loudoun County boundary to slightly west of the Route 28 (Sully Road) interchange, a distance of 4.25 miles. This document examines the safety and traffic operations for Existing Year 2020, plus travel forecasting and traffic operations for 2040 No-Build and Build alternatives. The traffic operations for all scenarios were evaluated using VISSIM. Using VISSIM allowed for the accurate simulation of driver behavior at the combination of signalized intersections, unsignalized driveways, and ramp merge and diverge areas along this study corridor. VISSIM also provides the level of control over the vehicle paths (i.e., lane changing behavior) between intersections that is required to simulate innovative intersection designs that could be considered along the corridor. The Existing conditions model development included the calibration process defined in the Virginia Department of Transportation (VDOT) Traffic Operations and Safety Analysis Manual (TOSAM) and VDOT VISSIM User Guide. Measures of effectiveness (MOEs) were reported for the 8 signalized intersections, 3 unsignalized intersections, 9 driveways, 11 ramp merge and diverge areas, 4 ramp weave sections, and 8 basic freeway segments. Figure 1 illustrates the overall project study area and shows the locations of the signalized intersections along the corridor.


Figure 1: Map of the Study Area

## 2. SAFETY EVALUATION

As part of this study, a crash analysis was performed along the corridor, using a seven-year crash dataset for the period (2013-2019) obtained from VDOT's Traffic Engineering Tableau Crash Analysis Tool, available online. The study area extends along Route 7 between Dranesville Road and Waverly Road, slightly west of the on/off ramps to/from Sully Road/Darrell Green Boulevard (Route 28). The crash analysis was performed to review patterns across the study area including on type of injury, collision type, travel direction, surface condition, and lighting conditions. Figure $\mathbf{2}$ and Figure $\mathbf{3}$ illustrate "heat maps" of the crashes reported within the study area between 2013 and 2019.

A total of 1,514 crashes occurred within the study area between 2013 and 2019; including 4 (less than $0.5 \%$ ) fatal injuries, 447 (approximately $30 \%$ ) injury related (including nonvisible, visible, and severe injuries) and 1063 (70\%) Property Damage Only (PDO) related crashes. During this 7 -year study period, there was an average of 216 crashes per year, which amounts to an average of 18 crashes per month along the entire corridor. Considering only the intersection-related crashes, there was an average of 135 crashes per intersection.

Analysis of the crash data resulted in the following insights:

- Approximately $59 \%$ of the total crashes were rear end crashes, $20 \%$ were angle crashes, and $9 \%$ were sideswipe crashes.
- $76 \%$ of the rear end collisions occurred along eastbound and westbound Route 7 approaching signalized intersections.
- $42 \%$ of the length of Route 7 within the study corridor is located within signalized intersections.
- Therefore, a disproportionate number of rear-end crashes occurred at signalized intersections, and there is a correlation between overall crash frequency and the prevalence of traffic signals along the corridor.
- Poor roadway conditions due to weather do not seem to be directly associated with the overall crash frequency; $82 \%$ of the total crashes were on dry roadway conditions, while only $16 \%$ of the crashes occurred on wet roadway conditions.
- 817 people were injured across the study area, including 8 pedestrians. $97(12 \%)$ people sustained severe injuries, 589 ( $72 \%$ ) people sustained visible injuries, and 127 ( $15 \%$ ) sustained non-visible injuries.
- 462 crashes occurred during the Fall (October-December), 372 crashes occurred during the winter (January-March), 314 crashes occurred during the spring (April-June), and 366 crashes occurred during the summer (July-September).
- More crashes occurred during November and December than any other month. When analyzing crashes occurring during the month of November, the majority of crashes occurred during the first half of the month as opposed to during the Thanksgiving holiday period. When analyzing crashes occurring during the month of December, there is a considerable spike in crashes slightly before Christmas and a dramatic decrease in crashes between Christmas and New Year Eve. Additionally, the analysis shows crashes were not higher during other holidays (Memorial Day, $4^{\text {th }}$ of July, Labor Day) when compared to the time periods surrounding the holidays.
- $104(7 \%)$ crashes were related to alcohol or drug consumption.
- The majority of the crashes (64\%) occurred under daylight conditions. For crashes occurring under nighttime conditions, $55 \%$ occurred were under lit conditions while $44 \%$ occurred were under not lit conditions.
- Crash frequency has decreased between 2013 and 2017. 2018 experienced the most crashes, followed by approximately a $25 \%$ reduction in crashes in 2019.
- Crash frequency was balanced between the eastbound and westbound directions, each of which adds up to $50 \%$ of the total crashes.

Crashes at the signalized intersections along the study area were further analyzed to attribute any localized safety issues related to the design context of each of the intersections. Table 1 to Table 8 summarize the crashes reported at each of the signalized intersections along the corridor between 2013 and 2019.

1. Route 7 at Dranesville Road:
a. Out of the 150 crashes, $58 \%$ were rear end approximately $30 \%$ were angle crashes.
b. $70 \%$ of the crashes are PDO crashes.
c. $67 \%$ of the crashes occurred during daylight conditions.
d. Intersection averages: 150 crashes, 21 crashes per year, 1.8 crashes per month
2. Route 7 at Lakeland Drive/Community Plaza:
a. Out of the 93 crashes at this location, $60 \%$ were rear end crashes.
b. $80 \%$ of the crashes are PDO crashes.
c. $67 \%$ of the crashes occurred during daylight conditions.
d. Intersection averages: 93 crashes, 12.3 crashes per year, 1.1 crashes per month
e.
3. Route 7 at Augusta Drive:
a. Out of the 107 crashes occurring at this location, approximately $70 \%$ were rear end crashes.
b. $70 \%$ of the crashes were PDO crashes.
c. One fatality occurred at this location, which was a pedestrian crash and was alcohol related.
d. Approximately $70 \%$ of crashes occurred during daylight conditions.
e. Intersection averages: 107 crashes, 15.3 crashes per year, 1.3 crashes per month
4. Route 7 at Cardinal Glen Circle/N Sterling Boulevard:
a. Out of the 140 crashes occurring at this intersection, $75 \%$ were rear-end crashes.
b. $75 \%$ of the crashes were also PDO crashes.
c. $75 \%$ of the crashes occurred on dry roadway conditions.
d. $55 \%$ of the crashes occurred during daylight conditions.
e. Intersection averages: 140 crashes, 20 crashes per year, 1.7 crashes per month
5. Route 7 at Potomac View Road:
a. Out of the 176 crashes occurring at this location, approximately $59 \%$ were rear end crashes and $25 \%$ were angle crashes.
b. Two pedestrian crashes occurred at this location, resulting in severe injuries, one of which was alcohol related, while the other one involving a senior citizen.
c. Intersection averages: 176 crashes, 25.1 crashes per year, 2 crashes per month
6. Route 7 at Campus Drive/Bartholomew Fair Drive:
a. Out of the 112 crashes occurring at this location, $60 \%$ were rear end crashes
b. Approximately $61 \%$ of the crashes were PDO crashes.
c. $70 \%$ of the crashes occurred during daylight conditions.
d. Approximately $87 \%$ of the crashes occurred under dry roadway surface conditions.
e. There were 2 pedestrian crashes occurring at this location, one in 2014 while the other in 2019, one of which resulted in a fatality and was alcohol related, while the other resulted in a severe injury and involved a senior citizen.
f. Intersection averages: 112 crashes, 16 crashes per year, 1.3 crashes per month
7. Route 7 at Palisade Parkway/Loudoun Tech Drive:
a. Out of 117 crashes occurring at this location, $55 \%$ were rear-end crashes.
b. Approximately $70 \%$ of the crashes were PDO crashes.
c. $77 \%$ of the crashes occurred on dry roadway surface conditions.
d. $60 \%$ of the crashes occurred during daylight conditions.
e. Intersection averages: 117 crashes, 16.7 crashes per year, 1.4 crashes per month
8. Route 7 at Countryside Boulevard/City Center Boulevard:
a. Out of 192 crashes occurring at this location, $63 \%$ were rear-end crashes.
b. One pedestrian crash occurred at this location, resulting in a visible injury.
c. Approximately $65 \%$ of the crashes were PDO crashes.
d. $84 \%$ of the crashes occurred on dry roadway conditions.
e. $60 \%$ of the crashes occurred during daylight conditions.
f. Intersection averages: 192 crashes, 27.4 crashes per year, 2.3 crashes per month

Based on the data for the intersection-related crashes, it appears that rear-end collisions have been the predominant crash type. Several studies have shown that the presence of traffic signals can lead to an increase in the frequency of rear-end crashes, particularly in areas with heavier volumes, so these trends are consistent with Route 7 within the study area. A review of Crash Modification Factors (CMF) available in the FHWA Clearinghouse database shows that roadway geometry is primarily a factor in crashes at signalized intersections only if it impairs drivers' visibility of the signal indications. Route 7 is mostly in a tangent section, and generally level, so the existing geometry is not likely the root cause of the most commonly occurring crashes along the corridor. The number of lanes can affect travel speed (i.e., traffic may travel at higher speeds if more lane capacity is available), and several CMFs show a correlation between higher speeds and increasing crash frequency. According to the CMF Clearinghouse, factors such as signal phasing, signal timing, and clearance intervals have a greater effect on crash frequency than roadway geometry.

The frequency of pedestrian-involved crashes was relatively low compared to the other crash types, and 2 of the 4 pedestrian crashes reported involved alcohol impaired pedestrians. Several intersections had a nighttime crash percentage of $40 \%$ or more, which suggests that street lighting should be reviewed for appropriateness of location and adequacy of brightness.


Figure 2: Crash Frequency Heat Map (2013-2019) along Route 7 East of Cascades Pkwy


Figure 3: Crash Frequency Heat Map (2013-2019) along Route 7 West of Cascades Pkwy

Table 1: Route 7 and Route 228 (Dranesville Road) Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface <br> Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 12 | 6 | 3 | 0 | 13 | 8 | 0 | 18 | 3 | 14 | 7 |
| 2014 | 16 | 4 | 1 | 0 | 13 | 8 | 0 | 16 | 5 | 14 | 7 |
| 2015 | 18 | 8 | 4 | 0 | 19 | 11 | 0 | 23 | 7 | 21 | 9 |
| 2016 | 5 | 6 | 2 | 0 | 10 | 3 | 0 | 11 | 2 | 8 | 5 |
| 2017 | 13 | 3 | 5 | 0 | 14 | 7 | 0 | 16 | 5 | 13 | 8 |
| 2018 | 11 | 7 | 3 | 0 | 21 | 0 | 0 | 18 | 3 | 14 | 7 |
| 2019 | 12 | 10 | 1 | 0 | 15 | 8 | 0 | 21 | 2 | 16 | 7 |
| Total | 87 | 44 | 19 | 0 | 105 | 45 | 0 | 123 | 27 | 100 | 50 |

Table 2: Route 7 and Lakeland Drive/Community Plaza Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 9 | 2 | 2 | 0 | 11 | 2 | 0 | 12 | 1 | 9 | 4 |
| 2014 | 8 | 2 | 1 | 0 | 9 | 2 | 0 | 10 | 1 | 6 | 5 |
| 2015 | 2 | 2 | 4 | 0 | 6 | 2 | 0 | 7 | 1 | 2 | 6 |
| 2016 | 9 | 5 | 1 | 0 | 10 | 5 | 0 | 12 | 3 | 10 | 5 |
| 2017 | 10 | 1 | 3 | 0 | 10 | 4 | 0 | 12 | 2 | 13 | 1 |
| 2018 | 11 | 5 | 1 | 0 | 15 | 2 | 0 | 13 | 4 | 10 | 7 |
| 2019 | 7 | 5 | 3 | 0 | 13 | 2 | 0 | 12 | 3 | 13 | 2 |
| Total | 56 | 22 | 15 | 0 | 74 | 19 | 0 | 78 | 15 | 63 | 30 |

Table 3: Route 7 and Augusta Drive Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/lcy | Daylight | Dark |
| 2013 | 18 | 4 | 0 | 0 | 16 | 6 | 0 | 21 | 1 | 14 | 8 |
| 2014 | 14 | 0 | 3 | 0 | 13 | 4 | 0 | 13 | 4 | 9 | 8 |
| 2015 | 6 | 2 | 0 | 1 | 4 | 4 | 1 | 6 | 3 | 6 | 3 |
| 2016 | 9 | 1 | 1 | 0 | 5 | 6 | 0 | 10 | 1 | 8 | 3 |
| 2017 | 9 | 3 | 3 | 0 | 10 | 5 | 0 | 13 | 2 | 13 | 2 |
| 2018 | 18 | 1 | 5 | 0 | 18 | 6 | 0 | 20 | 4 | 19 | 5 |
| 2019 | 3 | 5 | 1 | 0 | 8 | 9 | 0 | 7 | 2 | 7 | 2 |
| Total | 77 | 16 | 13 | 1 | 74 | 40 | 1 | 90 | 17 | 76 | 31 |

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Table 4: Route 7 and Cardinal Glen Circle/N Sterling Boulevard Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 18 | 0 | 0 | 0 | 11 | 7 | 0 | 14 | 4 | 11 | 7 |
| 2014 | 8 | 5 | 2 | 0 | 10 | 5 | 0 | 13 | 2 | 8 | 7 |
| 2015 | 10 | 3 | 1 | 0 | 11 | 3 | 0 | 14 | 0 | 8 | 6 |
| 2016 | 19 | 2 | 1 | 0 | 13 | 9 | 0 | 16 | 6 | 9 | 13 |
| 2017 | 20 | 5 | 1 | 0 | 21 | 5 | 0 | 14 | 12 | 11 | 15 |
| 2018 | 17 | 8 | 3 | 0 | 24 | 4 | 0 | 21 | 7 | 19 | 9 |
| 2019 | 13 | 2 | 2 | 0 | 14 | 3 | 0 | 12 | 5 | 12 | 5 |
| Total | 105 | 25 | 10 | 0 | 104 | 36 | 0 | 104 | 36 | 78 | 62 |

Table 5: Route 7 and Potomac View Road Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 17 | 10 | 3 | 0 | 18 | 12 | 0 | 28 | 2 | 19 | 11 |
| 2014 | 14 | 4 | 4 | 0 | 17 | 5 | 0 | 18 | 4 | 12 | 10 |
| 2015 | 13 | 5 | 5 | 0 | 17 | 6 | 0 | 18 | 5 | 10 | 13 |
| 2016 | 10 | 7 | 7 | 0 | 18 | 6 | 0 | 21 | 3 | 15 | 9 |
| 2017 | 13 | 10 | 2 | 0 | 16 | 9 | 0 | 23 | 2 | 17 | 8 |
| 2018 | 21 | 5 | 2 | 2 | 17 | 13 | 0 | 25 | 5 | 23 | 7 |
| 2019 | 15 | 3 | 4 | 0 | 18 | 4 | 0 | 19 | 3 | 13 | 9 |
| Total | 103 | 44 | 27 | 2 | 121 | 55 | 0 | 152 | 24 | 109 | 67 |

Table 6: Route 7 and Campus Drive/Bartholomew Fair Drive Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 8 | 2 | 2 | 0 | 8 | 4 | 0 | 9 | 3 | 8 | 4 |
| 2014 | 12 | 2 | 4 | 1 | 14 | 4 | 1 | 17 | 2 | 10 | 9 |
| 2015 | 6 | 4 | 4 | 0 | 9 | 5 | 0 | 10 | 4 | 8 | 6 |
| 2016 | 12 | 5 | 4 | 0 | 12 | 9 | 0 | 14 | 7 | 17 | 4 |
| 2017 | 10 | 2 | 2 | 0 | 8 | 6 | 0 | 13 | 1 | 11 | 3 |
| 2018 | 15 | 2 | 2 | 0 | 11 | 8 | 0 | 18 | 1 | 17 | 2 |
| 2019 | 5 | 6 | 1 | 1 | 7 | 6 | 0 | 12 | 1 | 7 | 6 |
| Total | 68 | 23 | 19 | 2 | 69 | 42 | 1 | 93 | 19 | 78 | 34 |

Table 7: Route 7 and Palisade Parkway/Loudoun Tech Drive Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 14 | 8 | 2 | 0 | 18 | 6 | 0 | 17 | 7 | 12 | 12 |
| 2014 | 10 | 2 | 6 | 0 | 13 | 5 | 0 | 17 | 1 | 8 | 10 |
| 2015 | 6 | 1 | 3 | 0 | 8 | 2 | 0 | 4 | 6 | 8 | 2 |
| 2016 | 12 | 3 | 5 | 0 | 14 | 6 | 0 | 16 | 4 | 10 | 10 |
| 2017 | 9 | 1 | 3 | 0 | 8 | 5 | 0 | 12 | 1 | 11 | 2 |
| 2018 | 7 | 1 | 5 | 0 | 10 | 3 | 0 | 10 | 3 | 8 | 5 |
| 2019 | 7 | 7 | 5 | 0 | 12 | 7 | 0 | 14 | 5 | 13 | 6 |
| Total | 65 | 23 | 29 | 0 | 83 | 34 | 0 | 90 | 27 | 70 | 47 |

Table 8: Route 7 and Countryside Boulevard/City Center Boulevard Crash Summary

| Year | Type |  |  |  | Crash Severity |  |  | Surface Condition |  | Light Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear End | Angle | Other | Pedestrian | PDO | Injury | Fatality | Dry | Wet/Icy | Daylight | Dark |
| 2013 | 14 | 6 | 9 | 0 | 13 | 16 | 0 | 23 | 6 | 15 | 14 |
| 2014 | 14 | 3 | 8 | 1 | 14 | 12 | 0 | 22 | 4 | 15 | 11 |
| 2015 | 19 | 4 | 6 | 0 | 21 | 8 | 0 | 23 | 6 | 11 | 18 |
| 2016 | 15 | 3 | 5 | 0 | 17 | 6 | 0 | 19 | 4 | 15 | 8 |
| 2017 | 16 | 5 | 4 | 0 | 16 | 9 | 0 | 22 | 3 | 17 | 8 |
| 2018 | 22 | 4 | 5 | 0 | 20 | 11 | 0 | 24 | 7 | 22 | 9 |
| 2019 | 21 | 4 | 4 | 0 | 22 | 7 | 0 | 27 | 2 | 18 | 11 |
| Total | 121 | 29 | 41 | 1 | 123 | 69 | 0 | 160 | 32 | 113 | 79 |

## 3. VISSIM MODEL CALIBRATION

The goal of the calibration effort for this study is to replicate the existing field conditions in the simulation model with minimal acceptable differences. The existing intersection turning movement volumes used for calibration and analysis are summarized in Appendix A. These volumes include all signalized intersections, unsignalized intersections, ramp merges and diverges, and driveways along Route 7 between Route 286 (Fairfax County Parkway) and Route 28 (Sully Road/Darrell Green Boulevard).

The VDOT VISSIM Users Guide and the VDOT Traffic Operations and Safety Analysis Manual, Version 2.0 (TOSAM) recommends following the calibration process as described in the FHWA Traffic Analysis Toolbox Volume III: Guidelines for Applying Traffic Microsimulation Modeling Software (FHWA-HRT-04-040).

The complete calibration memorandum and results are summarized in Appendix B.

## 4. EXISTING CONDITIONS OPERATIONAL ANALYSIS

Traffic analyses were performed using VISSIM to evaluate the current intersection and roadway performance along Route 7 under existing conditions. The purposes of the existing conditions analyses are to calibrate the simulation model based on field-measured data and to establish a baseline to which the future year No-Build conditions can be compared. Furthermore, since the safety evaluation of crash history along the corridor is based on past and existing conditions, the existing conditions operational analyses makes it possible to identify potential correlations between traffic operations and the types and frequency of crashes. Existing traffic performance was measured in terms of delay (seconds per vehicle) and levels of service (LOS) at intersections by individual turning movement, directional approach, and whole intersection. The performance of interchange ramp merges, diverges, and weaves was measured in terms of LOS based on density (vehicles per mile per lane, or vpmpl).

Field-measured turning movement counts for all the intersections and ramps along Route 7 within the study area were collected in June 2019. The traffic count volumes at the signalized intersections along the study corridor are shown in Figure 4. Signal phasing and timing programs were obtained from VDOT in the form of Synchro software files (VDOT plans to implement new signal timing programs along this portion of Route 7 in the near future; the original 2020 implementation date was delayed due to the COVID-19 pandemic). The Existing Conditions AM and PM peak hour levels of service (LOS) for each individual turning movement, directional approach, and whole intersection at the signalized locations along Route 7 are summarized in Figure 5. Tables showing the VISSIM analysis results for the Existing Conditions are provided in Appendix C.

Figure 4: Existing Conditions AM (PM) Peak Hour Volumes at Signalized Intersections


Figure 5: Existing Conditions AM (PM) Peak Hour Levels of Service (LOS)


Existing Conditions - Intersection Delays and HCM Levels of Service (LOS):

- Results were generated using VISSIM and measured for each overall signalized intersection, each directional approach at signalized and unsignalized intersections and driveways, and each individual turning movement.
- There are no overall intersections currently operating any worse than LOS D during either the AM or PM peak hours.
- There are no Route 7 directional approaches (i.e., eastbound or westbound approaches) at signalized intersections currently operating worse than LOS D during either the AM or PM peak hours.
- Signalized cross-street directional approaches that currently operate at LOS E or LOS F include:
- City Center Blvd/Countryside Blvd: NB LOS E (AM); SB LOS E (PM)
- Palisades Pkwy/Loudoun Tech Dr: NB LOS E (PM)
- Campus Dr/Bartholomew Fair Dr: SB LOS F (AM \& PM)
- Potomac View Road: NB LOS F \& SB LOS E (AM); NB LOS E \& SB LOS E (PM)
- N Sterling Blvd/Cardinal Glen Cir: SB LOS E (AM \& PM)
- Augusta Dr: SB LOS E (AM)
- Lakeland Dr/Community Plaza: SB LOS E (AM); NB LOS E \& SB LOS E (PM)
- Route 228 (Dranesville Rd)/Popeyes: NB LOS E \& SB LOS F (AM), NB LOS F \& SB LOS F (PM)
- Unsignalized (non-driveway) cross-street directional approaches that currently operate at LOS E or F include:
- Cedar Dr: NB LOS E \& SB LOS F (AM)
- Unsignalized driveway approaches that currently operate at LOS E or F include:
- Driveway from Mirror Ridge Shopping Center: SB LOS F (PM)
- Driveway from Cascades Village and Rehabilitation Center: NB LOS F (AM)
- Driveway to Christ the Redeemer Catholic Church: NB LOS F (AM)
- Driveway from Chick-fil-A: NB LOS F (AM)


## Existing Conditions - Intersection Queue Lengths:

- Maximum queue lengths were generated using VISSIM and measured in feet for each turning movement lane group (i.e., left turn, though, and right turn) at each signalized intersection, unsignalized intersection, and driveway.
- Queue lengths for left or right turn lane groups were compared to the available queue storage distance at each intersection.
- Queue lengths for the through lane groups were compared to the distance to the adjacent upstream intersection
- Intersections with maximum queues that currently exceed the available storage along Route 7 include:
- AM Peak Hour
- Potomac View Rd: EB Thru
- Cedar Dr (unsignalized): EB Thru; EB Right
- PM Peak Hour
- Potomac View Rd: WB Left
- N Sterling Blvd/Cardinal Glen Cir: EB Right; WB Thru
- Cedar Dr (unsignalized): WB Right
- Community Plaza/Lakeland Dr: WB Thru
- Route 228 (Dranesville Rd): WB Left

Existing Conditions - Grade-Separated Interchange HCM Levels of Service (LOS):
Highway Capacity Manual (HCM) levels of service (LOS) for basic freeway segments, ramp merge/diverge areas, and weave sections are based on density measured as passenger cars per mile per lane (pcpmpl), whereas VISSIM generates density as vehicles per mile per lane (vpmpl), which may be lower than pcpmpl . Therefore, using VISSIM density with the HCM LOS thresholds can yield results that are slightly better than using HCM density, although for Route 7, little difference is expected due to trucks being a low percentage (2\%) of the total traffic volume.

- Generated using VISSIM and measured for each on-ramp merge area, off-ramp diverge area, weaving area, and basic freeway segments between off- and on-ramps within each interchange.
- Ramp merge, diverge, weave, and basic freeway segments along Route 7 that currently operate at LOS E based on density (vehicles per mile per lane) include:
- Cascades Pkwy
- EB basic freeway segment (downstream) - AM
- EB on-ramp merge - AM
- WB on-ramp merge - PM
- No merge, diverge or weave, segments currently operate at LOS F.


## Existing Conditions - Analysis Conclusions:

- All 8 signalized intersections along this corridor have at least one directional approach that operates at LOS E or F during the AM and/or PM peak hours.
- All 3 unsignalized intersections and all nine (9) driveways operate at LOS D or better during both the $A M$ and $P M$ peak hours.
- 3 of the 5 roadway segments along eastbound Route 7 through the Cascades Pkwy interchange operate at LOS C or better during the AM, and all 5 segments are LOS C or better during the PM.
- All 5 roadway segments along westbound Route 7 through the Cascades Pkwy interchange operate at LOS C or better during the AM, and 4 of 5 segments are LOS C or better during the PM.
- There are 4 overflowing left or right turn storage lane maximum queues that exceed the available storage lengths during the AM peak hour, and 8 during the PM peak hour.
- During the AM peak hour, 1 of the 4 overflowing turn lanes is along Route 7, and during the PM peak hour, 3 of the 8 overflowing turn lanes are along Route 7; the remaining overflowing turn lanes are on the cross street approaches.


## 5. TRAVEL FORECASTING

The Loudoun County Department of Transportation and Capital Infrastructure (DTCI) established 2040 to be the design year for the Route 7 Concept Study. A review of historical traffic counts performed along Route 7 by VDOT and the roadway link volumes estimated by the Loudoun County Travel Demand Model was used to determine a reasonable long-term traffic growth rate. The review process was as follows:

- Using historical VDOT volume counts and estimates:
- Year 2014 bidirectional AADT $=58,000 \mathrm{vpd}$; Year 2019 bidirectional AADT $=59,000 \mathrm{vpd}$
- Annual growth rate between 2014 and $2019=+0.4 \%$ (or +0.004 )
- Examining the period from 2007 to 2018, the long-term historical trend shows a traffic reduction of about -2\% per year
- Using the Loudoun County Travel Demand Model:
- Year 2016 bidirectional ADT $=64,425 \mathrm{vpd}$; Year 2040 bidirectional ADT $=80,825 \mathrm{vpd}$
- Annual growth rate between 2016 and 2040 (for exponential growth calculation) $=+1 \%$
- Conclusions:
- Long-term historical trend was negative
- Short-term historical trend is positive but almost flat
- Long-term trend from the travel demand model is slightly positive
- Recommendation:

○ Use $\mathbf{+ 1 \%}$ annual growth to adjust Existing traffic counts to Year $\mathbf{2 0 4 0}$ levels for analysis
The chart shown in Figure 6 shows the growth projections associated with using long-term (2007-2019) historical VDOT volume data, recent short-term (2014-2019) historical VDOT volume data, base year (2016) and horizon year (2040) volume estimates from the Loudoun County Travel Demand Model, and a $+1 \%$ annual growth rate applied to the most recent (2019) VDOT AADT volume estimate on Route 7 within the study limits. The projected 2040 AADT volume using the recommended $+1 \%$ annual growth rate falls approximately midway between the trendline projections using the short-term recent historical VDOT volume data and the Loudoun County Model.


Figure 6: Comparison of Traffic Forecasting Methods
The projected 2040 intersection turning movement volumes and interchange volumes (including ramp junctions located immediately beyond the limits of any potential roadway improvements) are summarized in figures provided in Appendix D.

## 6. 2040 NO-BUILD CONDITIONS OPERATIONAL ANALYSIS

VISSIM was used to analyze the anticipated traffic operations along Route 7 in 2040 using the projected traffic volumes described in the previous section of this report (also shown in Figure 7). For these analyses, the traffic signal phasing and timing programs along Route 7 were maintained from the Existing Conditions analysis. No geometric roadway improvements were assumed to occur along Route 7 for this No-Build Conditions analysis. The purpose of this analysis is to establish the design year baseline operating conditions and support the concept development process for the Build Alternative by identifying specific locations along the corridor where capacity improvements may be needed. The 2040 No-Build Conditions AM and PM peak hour levels of service (LOS) for each individual turning movement, directional approach, and whole intersection at the signalized locations along Route 7 are summarized in Figure 8. Tables showing the VISSIM analysis results for the 2040 No-Build Conditions are provided in Appendix E.

## 2040 No-Build Conditions - Intersection Delays and HCM Levels of Service (LOS):

- Results were generated using VISSIM and measured for each overall signalized intersection, each directional approach at signalized and unsignalized intersections and driveways, and each individual turning movement.
- All intersections ( 8 signalized, 3 unsignalized, and 9 driveways) would operate at LOS $D$ during the AM or PM peak hours with the exception of the signalized Dranesville Rd intersection which would operate at LOS E during the PM peak hour.
- All of the eastbound and westbound approaches along Route 7 at signalized intersections would operate at LOS D or better during the AM and PM peak hours, with the following exceptions:
- Eastbound at Bartholomew Fair Dr/Campus Dr-LOS E during the AM peak hour
- Eastbound at Loudoun Tech Dr/Palisades Pkwy - LOS E during the PM peak hour
- Signalized cross-street directional approaches that would operate at LOS E or LOS F include:
- City Center Blvd/Countryside Blvd: NB LOS E (AM); SB LOS E (PM)
- Palisades Pkwy/Loudoun Tech Dr: NB LOS E (AM \& PM)
- Campus Dr/Bartholomew Fair Dr: SB LOS F (AM \& PM)
- Potomac View Road: NB LOS F \& SB LOS E (AM); NB LOS E \& SB LOS F (PM)
- N Sterling Blvd/Cardinal Glen Cir: SB LOS E (AM \& PM)
- Augusta Dr: SB LOS E (AM \& PM)
- Lakeland Dr/Community Plaza: SB LOS F (AM); NB LOS E \& SB LOS E (PM)
- Route 228 (Dranesville Rd)/Popeyes: NB LOS E \& SB LOS F (AM), NB LOS F \& SB LOS F (PM)
- Unsignalized (non-driveway) cross-street approaches that would operate at LOS E or F include:
- Cedar Dr: NB LOS F \& SB LOS F (AM); NB LOS F \& SB LOS F (PM)

Figure 7: 2040 No-Build Conditions AM (PM) Peak Hour Volumes at Signalized Intersections


Figure 8: 2040 No-Build Conditions AM (PM) Peak Hour Levels of Service (LOS)


- Unsignalized driveway approaches that would operate at LOS E or F include:
- Driveway from Mirror Ridge Shopping Center: SB LOS F (PM)
- Driveway from Cascades Village and Rehabilitation Center: NB LOS F (AM)
- Driveway to Christ the Redeemer Catholic Church: NB LOS F (AM)
- Driveway from Chick-fil-A: NB LOS F (AM \& PM)


## 2040 No-Build Conditions - Intersection Queue Lengths:

- Maximum queue lengths were generated using VISSIM and measured in feet for each turning movement lane group (i.e., left turn, though, and right turn) at each signalized intersection, unsignalized intersection, and driveway.
- Queue lengths for left or right turn lane groups were compared to the available queue storage distance at each intersection.
- Queue lengths for the through lane groups were compared to the distance to the adjacent upstream intersection
- Intersections with maximum queues that currently exceed the available storage along Route 7 include:
- AM Peak Hour
- Loudoun Tech Dr/Palisades Pkwy: EB Thru
- Campus Dr/Bartholomew Fair Dr: EB Thru
- Potomac View Rd: EB Thru; WB Left
- N Sterling Blvd/Cardinal Glen Cir: EB thru
- Augusta Dr: EB Thru
- Cedar Dr (unsignalized): EB Thru; EB Right
- PM Peak Hour
- City Center Blvd/Countryside Blvd: WB Thru
- Loudoun Tech Dr/Palisades Pkwy: EB Left
- Potomac View Rd: EB Left; WB Left
- N Sterling Blvd/Cardinal Glen Cir: EB Right; WB Thru
- Augusta Dr: SB Right; WB Thru
- Cedar Dr (unsignalized): EB Right; WB Thru
- Community Plaza/Lakeland Dr: WB Thru
- Route 228 (Dranesville Rd): WB Left


## 2040 No-Build Conditions - Grade-Separated Interchange HCM Levels of Service (LOS):

Highway Capacity Manual (HCM) levels of service (LOS) for basic freeway segments, ramp merge/diverge areas, and weave sections are based on density measured as passenger cars per mile per lane ( pcpmpl ), whereas VISSIM generates density as vehicles per mile per lane (vpmpl), which may be lower than pcpmpl. Therefore, using VISSIM density with the HCM LOS thresholds can yield results that are slightly better than using HCM density, although for Route 7, little difference is expected due to trucks being a low percentage (2\%) of the total traffic volume.

- Results were generated using VISSIM and measured for each on-ramp merge area, off-ramp diverge area, weaving area, and basic freeway segments between off- and on-ramps within each interchange.
- Ramp merge, diverge, weave, and basic freeway segments along Route 7 that would operate at LOS E based on density (vehicles per mile per lane) include:
- Cascades Pkwy
- EB off-ramp diverge - AM
- EB basic freeway segment (downstream) - AM
- EB weaving segment - AM
- EB basic freeway upstream (upstream) - AM
- EB on-ramp merge - AM
- WB on-ramp merge - PM


## 2040 No-Build Conditions - Analysis Conclusions:

- All 8 signalized intersections would continue to operate at a minimum LOS D, except for the intersection at Dranesville Road which would operate at LOS E during the PM peak hour.
- Like the Existing Conditions, every signalized intersection (8 total) along this corridor has at least one directional approach that would operate at LOS E or F during the AM and/or PM peak hours.
- All of the unsignalized intersections ( 3 total) and driveways ( 9 total) would operate at LOS D or better during the AM and PM peak hours.
- All 5 roadway segments along eastbound Route 7 through the Cascades Pkwy interchange would operate at LOS E or F during the AM, but all 5 segments would be LOS C or better during the PM.
- All 5 roadway segments along westbound Route 7 through the Cascades Pkwy interchange would operate at LOS C or better during the AM, and 3 of 5 segments are LOS C or better during the PM.
- Cedar Lane is the only unsignalized intersection (out of 3 along the corridor) that would have storage lanes with maximum queues that exceed the available storage length.


## 7. CONCEPT DEVELOPMENT FOR THE BUILD ALTERNATIVES

The existing and future No-Build conditions along Route 7 consist of conventional signalized and unsignalized at-grade intersections, as well as ramp merge, diverge, and weave sections within the Cascades Parkway and Atlantic Boulevard/Algonkian Parkway interchanges. Based on observations as well as the traffic operations analysis results presented in this study for the existing and future No-Build conditions, there are safety and performance deficiencies along this corridor that may require unconventional solutions. Therefore, an early step in the concept development process was to use the VDOT Junction Screening Tool (vJuST) to help identify innovative intersection and interchange configurations that might be appropriate and feasible along the Route 7 corridor. The results of this initial evaluation are summarized in Appendix F.

## Alternative 1: Modified Superstreet Corridor

Based in part on the results of this initial screening, but also considering the projected capacity needs, estimated costs, and right of way limitations, the project team developed Alternative 1 as a corridor of several modified Restricted Center U-Turn (RCUT) intersections, also referred to as a modified Superstreet configuration. The primary purpose of this proposed configuration is to reduce delay and improve peak direction travel times for through traffic along Route 7, while improving safety through the reduction of the number of conflict points at the signalized cross-street intersections. Due to the intersection spacing limitations identified during the vJuST analysis, the traditional Superstreet configuration, which would typically accommodate all required U-turn movements at new signalized intersections located between the existing signalized cross-street intersections, was modified to accommodate some U-turns at the downstream existing signalized cross-street intersections. This was done where the distance between existing signalized cross-street intersections was insufficient for inserting a new U-turn-only intersection between them. Alternative 1 adds four new traffic signals along Route 7 where it was feasible based on the spacing between the existing signalized intersections, resulting in a total of 12 signalized intersections within the study corridor.

In addition to converting the Route 7 corridor to a modified Superstreet configuration within the study limits, Alternative 1 also assumes the existing cloverleaf interchange at Route 7 and Cascades Parkway would be replaced with a Tight Diamond Interchange (TDI), where the on- and off-ramps to and from Route 7 would be signalized at closely-spaced ramp terminal intersections along Cascades Parkway. The primary goals of this interchange reconfiguration are to reduce the number of ramp junctions along Route 7 and eliminate the weave sections along Route 7 within the interchange, thereby improving safety and reducing delay with fewer conflict points. Figure 9 to Figure $\mathbf{1 1}$ show the Alternative 1 concept. Additional build alternatives may be developed in the future depending on the outcome of Loudoun County DTCI's review of the Alternative 1 benefits and challenges, including the traffic analysis results.

## 8. 2040 BUILD ALTERNATIVE OPERATIONAL ANALYSIS

Traffic operations for the Build alternatives described in the previous section of this report were analyzed using Synchro and VISSIM. The redistributed traffic volumes corresponding to Alternative 1 are shown in Figure 12. Synchro was used solely to determine the phasing and splits for any proposed signals associated with the Build alternatives and to optimize all the signals (existing and proposed) to minimize delay and maintain progression along Route 7. These optimized signal timing plans were subsequently imported into VISSIM, since VISSIM does not have automatic signal timing optimization capabilities. VISSIM was used to perform microsimulation analysis of traffic operations, evaluating the following measures of effectiveness (MOEs): Average and maximum queue lengths, delays in second per vehicle by intersection, directional approach, and individual turning movement, and HCM-based levels of service (LOS) by intersection, directional approach, and individual turning movement. These analyses were performed based on the projected AM and PM peak hours on a typical weekday in 2040. The 2040 Alternative 1 AM and PM peak hour levels of service (LOS) for each individual turning movement, directional approach, and whole intersection at the signalized locations along Route 7 are summarized in Figure 13. Tables showing the VISSIM analysis results for the 2040 No-Build Conditions are provided in Appendix G.

## Alternative 1: Modified Superstreet Corridor - Analysis Results

## Alternative 1 Intersection Delays and HCM Levels of Service (LOS):

- 9 existing and proposed signalized intersections along Route 7 would operate at LOS D or better during the AM or PM peak hours. Exceptions are as follows:
- Bartholomew Fair Dr / Campus Dr - LOS E during the AM peak hour
- Community Plaza / Lakeland Dr - LOS E during the PM peak hour
- Dranesville Rd - LOS F during the PM peak hour
- 20 of the 24 total eastbound and westbound Route 7 approaches at signalized intersections would operate at LOS D or better during the AM or PM peak hours, with the following exceptions:
- Eastbound at Bartholomew Fair Dr/Campus Dr - LOS F during the AM peak hour
- Westbound at the new U-turn crossover west of $N$ Sterling Blvd - LOS F during the AM peak hour
- Westbound at Lakeland Dr-LOS F during the PM peak hour
- Westbound at Dranesville Rd - LOS F during the PM peak hour
- Signalized cross-street directional approaches that would operate at LOS E or LOS F include:
- City Center Blvd/Countryside Blvd: NB LOS F \& SB LOS E (AM); NB LOS E (PM)
- Davenport Dr (new signal): SB LOS F (AM \& PM)
- Palisades Pkwy/Loudoun Tech Dr: NB LOS E \& SB LOS E (AM)
- Campus Dr/Bartholomew Fair Dr: NB LOS F (AM \& PM)
- Potomac View Road: SB LOS F (AM); SB LOS E (PM)
- N Sterling Blvd/Cardinal Glen Cir: SB LOS F (AM)




Figure 12: 2040 Build Alternative 1 AM (PM) Peak Hour Volumes at Signalized Intersections


Figure 13: 2040 Build Alternative 1 AM (PM) Peak Hour Levels of Service (LOS)


- Augusta Dr: SB LOS E (AM)
- Cedar Dr (new signal): NB LOS E (AM); NB LOS F \& SB LOS F (PM)
- Lakeland Dr/Community Plaza: SB LOS F (AM); SB LOS E (PM)
- Dranesville Rd: NB LOS F (AM \& PM)
- Unsignalized driveway approaches that would operate at LOS E or $F$ include:
- Driveway from Mirror Ridge Shopping Center: LOS E (PM)
- Driveway from Cascades Village and Rehabilitation Center: NB LOS F (AM); NB LOS E (PM)
- Driveway east of Dranesville Rd: NB LOS F (PM)


## Alternative 1 Intersection Queue Lengths:

Maximum queue lengths for Alternative 1 were generated using VISSIM and measured in feet for each turning movement lane group (i.e., left turn, though, and right turn) at each signalized intersection, unsignalized intersection, and driveway. Queue lengths for left or right turn lane groups were compared to the existing available queue storage distance at each existing intersection. At the proposed signalized locations added for the Alternative 1 concept, the available queue storage distances were maximized based on the available distance to the upstream intersection. Queue lengths for the through lane groups were compared to the distance to the adjacent upstream intersection. Results show that through lane queues at several signalized intersections would extend back through the upstream intersection. This is not due to the through lane volumes; it is caused by the left-turn or right-turn lane queues overflowing into the adjacent through lanes. Resolving the turn lane storage issues at the locations listed below would indirectly solve the through lane queuing issues. The Alternative 1 analyses performed for this study already assume optimized signal timing for the turning movements; therefore, the recommended storage lane lengths may need to be longer than what were assumed, if feasible based on intersection spacing.

- Signalized intersections with maximum turn lane queues along Route 7 that are projected to exceed the available storage include:
- AM Peak Hour
- City Center Blvd/Countryside Blvd: EB Left; WB Left
- Davenport Dr (new signal): EB U-turn
- Loudoun Tech Dr/Palisades Pkwy: EB Left; WB Left
- Campus Dr/Bartholomew Fair Dr: EB Left; WB U-turn
- Potomac View Rd: EB Left; WB Left
- U-turn Crossover west of $N$ Sterling Blvd (new signal): WB U-turn
- N Sterling Blvd/Cardinal Glen Cir: EB Left; WB Left
- U-turn Crossover west of Augusta Dr (new signal): WB U-turn
- Augusta Dr: WB Thru; WB U-turns
- Cedar Dr (new signal): EB Right; WB Left; WB Right
- PM Peak Hour
- City Center Blvd/Countryside Blvd: EB Left; WB Left
- Davenport Dr (new signal): EB U-turn; WB U-turn
- Loudoun Tech Dr/Palisades Pkwy: WB Left
- Campus Dr/Bartholomew Fair Dr: EB Left; WB Right
- Potomac View Rd: EB Left; WB Left; WB Right
- U-turn Crossover west of Augusta Dr (new signal): WB Thru
- Augusta Dr: WB U-turn
- Cedar Dr (new signal): EB Right; WB Right
- Community Plaza/Lakeland Dr: WB Left
- Route 228 (Dranesville Rd): WB Left


## Alternative 1 Grade-Separated Interchange HCM Levels of Service (LOS):

Highway Capacity Manual (HCM) levels of service (LOS) for basic freeway segments and ramp merge/diverge areas are based on density measured as passenger cars per mile per lane (pcpmpl), whereas VISSIM generates density as vehicles per mile per lane (vpmpl), which may be lower than pcpmpl. Therefore, using VISSIM density with the HCM LOS thresholds can yield results that are slightly better than using HCM density, although for Route 7, little difference is expected due to trucks being a low percentage (2\%) of the total traffic volume.

Results were generated using VISSIM and measured for each on-ramp merge area, off-ramp diverge area, and basic freeway segments between off- and on-ramps within the Cascades Parkway interchange, reconfigured as a tight diamond interchange (TDI) under Alternative 1.

- Ramp merge, diverge, and basic freeway segments along Route 7 that would operate at LOS E or LOS F based on density (vehicles per mile per lane) include:
- EB basic freeway segment (between the off- and on-ramps) - LOS E (AM)
- EB on-ramp merge - LOS E (AM)
- WB on-ramp merge - LOS E (PM)


## Alternative 1 Safety Impacts

- The review of the recent crash history and trends along Route 7 between Dranesville Road and Route 28 showed that a disproportionate number of rear-end crashes have occurred at signalized intersections.
- 42 percent of the length of Route 7 within the study corridor lies within the boundaries of the signalized intersections along the corridor.
- 76 percent of the rear-end crashes within the study corridor occurred at signalized intersections.
- 59 percent of all reported crashes within the study corridor were rear-end crashes; therefore, there is a correlation between crash frequency and the prevalence of signalized intersections along the corridor.
- Alternative 1 would reduce the number of conflict points at each of the existing signalized intersections by prohibiting crossing traffic and left-turns from the side streets.
- However, Alternative 1 would also add 6 new traffic signals to accommodate the movements displaced by restricting these cross-street movements.


## Alternative 1 Analysis Conclusions:

- Even with the proposed conversion to a Green-T configuration, the Dranesville Road intersection would continue to be the worst-performing intersection along the Route 7 study corridor in terms of overall level of service, operating at LOS F during the PM peak hour.
- Looking at the performance of the individual turning movements at each signalized intersection, 22 of the 24 straight through movements along eastbound and westbound Route 7 would operate at LOS D or better. Exceptions include:
- Eastbound through movement at Bartholomew Fair Dr/Campus Dr - LOS F during the AM
- Westbound through movement at Dranesville Rd and at Community Plaza/Lakeland Dr LOS F during the PM
- With through and left-turn traffic from the cross-streets diverted as right-turns to new downstream U-turn signals for this modified superstreet configuration, most of the excessive

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delays and poor levels of service (i.e., LOS E or LOS F) would occur for the left, right, and U-turn movements along Route 7 and for the cross-streets approaching Route 7.

- All 22 left and U-turn movements at the signalized intersections along eastbound and westbound Route 7 would operate at LOS E or F during the AM and/or PM peak hours.
- 13 of the 17 total cross-street approaches at signalized intersections within the study corridor would operate at LOS E or F during the AM and/or PM peak hours.

Additional build alternatives may be developed in the future depending on the outcome of Loudoun County DTCl's review of the Alternative 1 benefits and challenges, including these traffic analysis results.

## 9. CONCLUSIONS

This traffic operations and safety report examines existing and projected future conditions along Route 7 in Loudoun County, Virginia, between Dranesville Rd (Route 228) at the Fairfax County line to the Route 28 interchange, a distance of approximately 4.25 miles. This study includes an evaluation of the history of reported crashes occurring during recent years, an analysis of traffic operations along the corridor under existing conditions, travel demand forecasts for a 2040 No-Build alternative and (to-date) one 2040 Build alternative, and an analysis of the traffic operations expected under those alternatives.

## Comparison of Alternative 1 to the No-Build Alternative

As part of the Route 7 Concept Study, several potential Build alternatives were developed at the sketch planning level and presented to Loudoun County DTCl staff and representatives from other government and institutional stakeholders during a brainstorming work session in August 2020. Of these potential improvement options, the Modified Superstreet Corridor was selected to be the first of several potential alternatives to be retained for more detailed analysis. This concept is referred to as Alternative 1.

The analysis of traffic operations under the No-Build alternative identified individual turning movements, directional approaches, and overall intersections that would likely perform unsatisfactorily (i.e., at level of service (LOS) E or LOS F) during the AM and/or PM peak hours in 2040. Table 9 and Table 10 compare the number of directional approaches and overall intersections that would operate at each level of service under the No-Build alternative and Alternative 1. Full tables comparing the delays by approach and intersection, as well as comparing the roadway segment LOS within interchange areas and the corridor travel times, are provided in Appendix H.

Table 9: Comparison of the Number of Approaches and Intersections at Each LOS - AM Peak Hour

| Level of Service | Directional Approaches |  |  |  | Overall Intersections |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2040 No-Build |  | 2040 Alternative 1 |  | 2040 No-Build |  | 2040 Alternative 1 |  |
|  | Number | \% of Total | Number | \% of Total | Number | \% of Total | Number | \% of Total |
| LOS F | 9 | 16\% | 12 | 20\% | 0 | 0\% | 1 | 5\% |
| LOS E | 5 | 9\% | 5 | 8\% | 0 | 0\% | 1 | 5\% |
| LOS D | 7 | 13\% | 7 | 12\% | 2 | 10\% | 2 | 9\% |
| LOS C | 12 | 21\% | 8 | 13\% | 6 | 30\% | 6 | 27\% |
| LOS B | 7 | 13\% | 7 | 12\% | 4 | 20\% | 3 | 14\% |
| LOS A | 16 | 29\% | 21 | 35\% | 8 | 40\% | 9 | 41\% |

Table 10: Comparison of the Number of Approaches and Intersections at Each LOS - PM Peak Hour

| Level of Service | Directional Approaches |  |  |  | Overall Intersections |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2040 No-Build |  | 2040 Alternative 1 |  | 2040 No-Build |  | 2040 Alternative 1 |  |
|  | Number | \% of Total | Number | \% of Total | Number | \% of Total | Number | \% of Total |
| LOS F | 8 | 14\% | 8 | 13\% | 0 | 0\% | 1 | 5\% |
| LOS E | 8 | 14\% | 4 | 7\% | 1 | 5\% | 1 | 5\% |
| LOS D | 5 | 9\% | 3 | 5\% | 2 | 10\% | 0 | 0\% |
| LOS C | 11 | 20\% | 13 | 22\% | 3 | 15\% | 6 | 27\% |
| LOS B | 6 | 11\% | 12 | 20\% | 4 | 20\% | 5 | 23\% |
| LOS A | 18 | 32\% | 20 | 33\% | 10 | 50\% | 9 | 41\% |

The comparison of the LOS analysis results summarized in the AM peak hour table shows that traffic operations would improve at some locations under Alternative 1 while they would worsen at other locations under Alternative 1. However, during the PM peak hour, there would not be much change in LOS for Alternative 1 compared to the No-Build alternative.

In terms of density on the Route 7 roadway segments through the Cascades Parkway interchange, the analysis results show an improvement (i.e., reduction) in the density (vehicles per mile per lane) with the tight diamond interchange (TDI) configuration proposed under Alternative 1. This is likely due to the removal of an on- and off-ramp in each direction along Route 7 and the corresponding elimination of the weaving segment between those ramps.

Examining the corridor end-to-end travel times along Route 7 shows that Alternative 1 would result in a substantial improvement (i.e., reduction) in travel time in the peak direction (eastbound) during the AM peak hour. The time required to travel the 4.25-mile study corridor eastbound would be reduced by more than 4 minutes - a $28 \%$ reduction in travel time. However, a comparison of the PM peak hour, peak direction (westbound) travel times shows that Alternative 1 would have no impact. The time required to travel the 4.25 -mile study corridor westbound would remain at 11 minutes for Alternative 1 - the same as under the No-Build alternative.

The addition of 6 new traffic signals along Route 7 to accommodate the movements displaced by Alternative 1's modified superstreet configuration may offset the crash-reducing benefits of eliminating some conflict points at the existing intersections. These existing conflict points would be reduced by prohibiting through and left-turn movements from the cross-streets at the existing signalized intersections along Route 7.

## Summary

There are several tangible benefits associated with Alternative 1 that are evident when comparing its performance to that of the No-Build alternative. However, there remain several areas where performance would decrease under Alternative 1, such as LOS for the cross-street approaches and for the proposed Uturn movements. Furthermore, the potential for crash reduction under Alternative 1 may be small.

## Appendix A:

2019 Balanced Traffic Volumes


## Existing 2019 Peak Hour Volumes



Route 7 at Jona Dr (Sunrise Senior Living)


Route 7 at Davenport Dr


## Existing 2019 Peak Hour Volumes



Route 7 at Shell Gas Station \& DD BBQ




## Existing 2019 Peak Hour Volumes



## Appendix B:

## Calibration Memorandum and Results

## VISSIM MODEL CALIBRATION

## Purpose and Introduction

Microscopic simulation tool VISSIM version 11.0 was used to model the study area for the Route 7 Concept Study from Route 28 to the Loudoun/Fairfax County Line in Loudoun County, Virginia. The simulation models were developed for the AM and PM peak hours and were calibrated using field travel times and traffic volumes, in order to replicate field conditions within acceptable tolerances and to produce accurate Measures of Effectiveness (MOEs).

The purpose of this memorandum is to document the calibration procedures that were used and the parameters that were changed for the Route 7 Concept Study from Route 28 to the Loudoun/Fairfax County Line.

## Calibration Setup

## Calibration Targets

The goal of the calibration effort is to replicate the existing field condition in the simulation model with minimal acceptable differences. The VDOT VISSIM Users Guide and the VDOT Traffic Operations and Safety Analysis Manual, Version 2.0 (TOSAM) recommends following the calibration process as described in the FHWA Traffic Analysis Toolbox Volume III: Guidelines for Applying Traffic Microsimulation Modeling Software (FHWA-HRT-04-040). Below is a list of recommended thresholds that were used for the calibration of the VISSIM model for the Route 7 Concept Study from Route 28 to the Loudoun/Fairfax County Line.

1. Simulated Traffic Volumes (vph), Model Versus Observed GEH Statistic < 5.0

The GEH statistic formula used for comparing model flows versus field flows and is computed as follows:

$$
G E H=\sqrt{\frac{2(m-c)^{2}}{(m+c)}}
$$

where:
$\mathrm{m}=$ model output traffic volume (vph)
$\mathrm{c}=$ input traffic volume (vph)
2. Simulated Travel Times (seconds)

Within $\pm 30 \%$ for average observed travel times on arterials
As mentioned in the FHWA Traffic Analysis Toolbox guidelines, the target values will vary according to the purpose for which the microsimulation model is being developed and the resources available to the analyst. It is important to note that when calibrating to low travel times or volumes, small absolute differences represent significant percentage deviations.

## VISSIM Global Parameters

The VDOT TOSAM describes specific VISSIM global parameters and inputs that must be coded into each model. These global parameters and their data sources are described below.

## Vehicle Inputs \& Seeding Time

The balanced traffic volumes for the peak hours are coded in the network. The peak hour (1-hour) duration is used for recording and processing the results. Additionally, a 15 -minute seeding time is coded to produce queue or traffic demand buildup. The equivalent hourly traffic volume for the first 15-minute interval is used for the seeding period during the AM and PM peak hour.

## Heavy Vehicle Percentages

The heavy vehicle percentage on Route 7 and Fairfax County Pkwy were determined based on field traffic counts (see Table 1). The heavy vehicle percentages for all the other minor roads are coded as 2\%.
Table 1: Heavy Vehicle Percentages

| Corridor | AM | PM |
| :---: | :---: | :---: |
| Route 7, EB | $2.7 \%$ | $0.7 \%$ |
| Route 7, WB | $3.0 \%$ | $2.2 \%$ |
| Fairfax County Pkwy, NB | $1.4 \%$ | $0.4 \%$ |
| Fairfax County Pkwy, SB | $0.3 \%$ | $2.7 \%$ |

## Arrival Distribution

The "exact volume" arrival distribution is used for all the vehicle inputs.

## Link Speeds \& Turning Speeds

A linear distribution ranging $+/-5 \mathrm{mph}$ from the posted speed limit is used in the network. As recommended in the TOSAM, a linear distribution range of $7.5-15.5 \mathrm{mph}$ is used for right turn speeds and 12.4-18.6 mph is used for the left-turns.

Origin-Destination (O-D)
The origin-destination routes were established based on the existing turning movement counts and later combined based on field observations to achieve realistic driver behavior.

## Simulation Period and Resolution

A simulation period of 4,500 seconds including 900 seconds of seeding time is used during the AM and PM peak hour. As recommended in TOSAM, a simulation resolution of 10 time steps/simulation second is used.

## VISSIM Default Driver Behavior Parameters

The VISSIM software models driver behavior based on the Wiedemann 74 and Wiedemann 99 car following models. The former model is recommended for modeling arterials or collector roadways and is used to model most of the roadways within the study area.

## Data Sources

Volume and travel time data were used to calibrate the VISSIM models.
Field-measured turning movement counts for all the intersections and ramps along Route 7 within the study area were collected in June 2019. The turning movement counts were balanced manually. The balanced traffic volume network for the study area is shown in Appendix A of the main report.

Travel time runs were performed during peak hours on February 26, February 27, and March 5, 2020, along Route 7 from Route 28 to Fairfax County Pkwy. Additionally, the travel times along the study corridor were also collected from INRIX. All field travel time runs were performed prior to the widespread school closures and shutdowns resulting from the COVID-19 pandemic.

According to TOSAM, for routes that span a long distance, travel time should be calibrated at both the segment level and corridor level. For the corridor level travel time calibration, the average travel times along the entire study corridor were retrieved from the field travel time runs and were used for calibration. For the segment level travel time calibration, since there are multiple traffic signals along the study corridor, the segment level travel time can vary significantly depending on if the vehicle is stopped by a red light during field data collection. Therefore, INRIX data were used for the segment level travel time calibration instead of field data. Note that the INRIX travel time at each segment is the average travel time for all the vehicles that travel through the segment, including both the through traffic and turning traffic. Therefore, the sum total of these segment travel times is greater than the corridor end-to-end travel time measured in the field using a test vehicle making no turns. The traffic signals along the corridor are typically timed to optimize progression for through traffic, not turning traffic, resulting in greater delays and longer travel times reported for the individual segments, which include times for all traffic including turning vehicles. Table 2 shows the processed travel time outputs.

Table 2: INRIX and Field-Measured Travel Times

| Corridor |  | From | To | AM Travel Time (s) | PM Travel Time (s) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte. 7 EB | Segments | Rte. 28 off ramp | Rte. 28 on ramp | 28 | 28 |
|  |  | Rte. 28 on ramp | City Center Blvd | 69 | 71 |
|  |  | City Center Blvd | Cascades Pkwy off ramp | 59 | 75 |
|  |  | Cascades Pkwy off ramp | Cascades Pkwy on ramp | 54 | 40 |
|  |  | Cascades Pkwy on ramp | North Sterling Boulevard | 250 | 141 |
|  |  | North Sterling Boulevard | Dranesville Road | 154 | 132 |
|  |  | Dranesville Road | Fairfax County Pkwy | 59 | 72 |
|  |  | Sum |  | 673 | 560 |
|  | Corridor | Rte. 28 off ramp | Fairfax County Pkwy | 561 | 451 |
| Rte. 7 <br> WB | Segments | Fairfax County Pkwy | Dranesville Road | 49 | 278 |
|  |  | Dranesville Road | North Sterling Boulevard | 111 | 216 |
|  |  | North Sterling Boulevard | Cascades Pkwy off ramp | 123 | 120 |
|  |  | Cascades Pkwy off ramp | Cascades Pkwy on ramp | 45 | 49 |
|  |  | Cascades Pkwy on ramp | City Center Blvd | 69 | 85 |
|  |  | City Center Blvd | Rte. 28 off ramp | 48 | 45 |
|  |  | Rte. 28 off ramp | Rte. 28 on ramp | 48 | 77 |
|  |  | Sum |  | 495 | 869 |
|  | Corridor | Fairfax County Pkwy | Rte. 28 on ramp | 455 | 494 |

Notes:

- Travel time for each segment is from INRIX data, and it is the average travel time for all the vehicles that travel through the segment, which include both the through traffic and turning traffic.
- Travel time for the entire corridor is from field data, and it is the average travel time for the field vehicle traveling through the entire corridor (i.e., end-to-end, making no turns)

Video footage was recorded along the corridor during the field travel time runs using a dashboardmounted camera. These videos were used to observe queue lengths along Route 7, and these observations aided the model calibration effort.

## Number of Model Runs

Ten (10) VISSIM model runs were performed for both the AM and PM models. The number of simulation runs were determined by the VDOT sample size determination tool, version 1.1. The measures of effectiveness (MOE) used in the tool is the corridor level travel time. The results of the VDOT sample size determination tool are summarized in an attachment to this memo.

## Calibration Process and Results

Initial simulation runs conducted using default driver behavior parameters showed that volume throughput calibration targets were generally met for all the study intersections. However, there are significant differences in travel time and queues along the study corridors, indicating that default driver behavior types do not replicate field conditions with sufficient accuracy. Hence, four (4) additional driving behavior types were created and applied to problematic segments/links. The driver behavior parameters for these four types of driving behavior types were adjusted through an iterative process to achieve results within the calibration targets. In particular, critical car following and lane changing parameters of the Wiedemann 74 model were adjusted for the calibration process. Additionally, the distribution for the desired speed limits were also adjusted.

The changes to the driver behavior model parameters and desired speed distribution yield model output that better matches the observed field conditions. All volume throughputs yield GEH statistic values within the recommended range (i.e., all GEH values are less than 5). Additionally, all travel times were calibrated to be within $30 \%$ of field collected travel times.

Modeled average and maximum queues were qualitatively assessed and were generally consistent with queues observed during field observations.

Table 3 summarizes the final calibrated model parameters that were used in the calibrated VISSIM models.

Table 3: Final Model Calibration Parameters

| Wiedemann 74 Following Parameter | Default | AM Driving Behavior Types |  |  |  | PM Driving Behavior Types |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM1 | AM2 | AM3 | AM4 | PM1 | PM2 | PM3 | PM4 |
| Average Standstill Distance (ft) | 6.56 | 6.56 | 7.2 | 8.0 | 8.6 | 6.56 | 7.7 | 8.0 | 8.7 |
| Additive part of safety distance (ft) | 2.0 | 2.0 | 2.2 | 3.0 | 3.6 | 2.0 | 2.7 | 3.0 | 3.7 |
| Multiplicative part of safety distance (ft) | 3.0 | 3.0 | 3.2 | 4.0 | 4.6 | 3.0 | 3.7 | 4.0 | 4.7 |
| Wiedemann 74 Lane Change Parameter |  |  |  |  |  |  |  |  |  |
| Safety Distance Reduction Factor | 0.6 | 0.3 | 0.3 | 0.6 | 0.3 | 0.6 | 0.3 | 0.6 | 0.3 |

The results for the calibrated models are attached to this memo.





Finalized AM
Finalized PM

| Corridor |  | From | To | INRIX \&Field Data <br> Travel Time (TT) |  | Model Data |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM |  |  |  | PM |  |
|  |  | Iteration-15 |  |  |  | Iteration-11 |  |
|  |  | AM |  | PM | TT | \% Diff | TT | \% Diff |
| Eastbound |  |  |  |  |  |  |  |  |  |
| Rte 7 | Segments |  | Rte. 28 off ramp | Rte. 28 on ramp | 28 | 28 | 28 | 1\% | 28 | 1\% |
|  |  |  | Rte. 28 on ramp | City Center Blvd | 69 | 71 | 74 | 7\% | 76 | 7\% |
|  |  |  | City Center Blvd | Cascades Pkwy off ramp | 59 | 75 | 60 | 2\% | 77 | 3\% |
|  |  | Cascades Pkwy off ramp | Cascades Pkwy on ramp | 54 | 40 | 48 | -12\% | 36 | -10\% |
|  |  | Cascades Pkwy on ramp | North Sterling Boulevard | 250 | 141 | 221 | -12\% | 153 | 8\% |
|  |  | North Sterling Boulevard | Dranesville Road | 154 | 132 | 150 | -3\% | 143 | 8\% |
|  |  | Dranesville Road | Fairfax County Pkwy | 59 | 72 | 55 | -8\% | 65 | -10\% |
|  |  | Sum |  | 673 | 560 | 635 | -6\% | 578 | 3\% |
|  | Corridor | Rte. 28 off ramp | Fairfax County Pkwy | 561 | 451 | 543 | -3\% | 470 | 4\% |
| Westbound |  |  |  |  |  |  |  |  |  |
| Rte 7 | Segments | Fairfax County Pkwy | Dranesville Road | 49 | 278 | 52 | 6\% | 296 | 6\% |
|  |  | Dranesville Road | North Sterling Boulevard | 111 | 216 | 117 | 5\% | 226 | 5\% |
|  |  | North Sterling Boulevard | Cascades Pkwy off ramp | 123 | 120 | 115 | -7\% | 122 | 2\% |
|  |  | Cascades Pkwy off ramp | Cascades Pkwy on ramp | 45 | 49 | 41 | -10\% | 48 | -1\% |
|  |  | Cascades Pkwy on ramp | City Center Blvd | 69 | 85 | 72 | 3\% | 87 | 2\% |
|  |  | City Center Blvd | Rte. 28 off ramp | 48 | 45 | 46 | -3\% | 47 | 5\% |
|  |  | Rte. 28 off ramp | Rte. 28 on ramp | 48 | 77 | 50 | 5\% | 73 | -5\% |
|  |  | Sum |  | 495 | 869 | 493 | 0\% | 899 | 3\% |
|  | Corridor | Fairfax County Pkwy | Rte. 28 on ramp | 455 | 494 | 405 | -11\% | 538 | 9\% |

## Note:

- Travel time at each segment is from INRIX data, and it is the average travel time for all the vehicles that travel through the segment, which include both the through traffic and turning traffic.
- Travel time for the entire corridor is from field data, and it is the average travel time that the field vehicle travel through the entire corridor

| Field data <br> Finalized AM <br> Finalized PM |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Movement | Field Data |  | Model Throughput |  |  |  |
|  |  | Traffic Volume |  | Iteration 15 |  | Iteration 11 |  |
|  |  |  |  | Traffic Volume | GEH | Traffic Volume $\mathrm{GEH}^{\text {a }}$ |  |
|  |  | AM | PM | AM |  | PM |  |
| Rte 7 at Rte 28 Interchange | Rte 7 EB to Rte 28 | 2585 | 1670 | 2571 | 0.28 | 1653 | 0.42 |
|  | Rte 28 to Rte 7 EB | 508 | 946 | 506 | 0.09 | 945 | 0.03 |
|  | Rte 7 WB to Rte 28 | 612 | 551 | 617 | 0.20 | 531 | 0.86 |
|  | Rte 28 to Rte 7 WB | 1731 | 2293 | 1733 | 0.05 | 2208 | 1.79 |
|  | Rte 7 EB Through | 2765 | 2288 | 2793 | 0.5 | 2308 | 0.4 |
|  | Rte 7 WB Through | 1737 | 3046 | 1708 | 0.7 | 2944 | 1.9 |
| Rte 7 at Broad Run Drive | WBRT | 18 | 30 | 18 | 0.0 | 31 | 0.2 |
|  | WBT | 1668 | 2991 | 1651 | 0.4 | 2890 | 1.9 |
|  | SBRT | 69 | 55 | 69 | 0.0 | 54 | 0.1 |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 EB to Atlantic Blvd NB | 365 | 724 | 375 | 0.5 | 722 | 0.1 |
|  | Rte 7 EB to Atlantic Blvd SB | 195 | 189 | 199 | 0.3 | 189 | 0.0 |
|  | Atlantic Blvd NB to Rte 7 EB | 43 | 78 | 44 | 0.2 | 82 | 0.4 |
|  | Atlantic Blvd SB to Rte 7 EB | 161 | 102 | 161 | 0.0 | 100 | 0.2 |
|  | Rte 7 WB to Atlantic Blvd NB | 53 | 119 | 53 | 0.0 | 116 | 0.3 |
|  | Rte 7 WB to Atlantic Blvd SB | 38 | 26 | 37 | 0.2 | 24 | 0.4 |
|  | Atlantic Blvd NB to Rte 7 WB | 52 | 288 | 51 | 0.1 | 286 | 0.1 |
|  | Atlantic Blvd SB to Rte 7 WB | 250 | 338 | 247 | 0.2 | 329 | 0.5 |
|  | Rte 7 EB Through | 2713 | 2321 | 2729 | 0.3 | 2339 | 0.4 |
|  | Rte 7 WB Through | 1996 | 2946 | 1978 | 0.4 | 2838 | 2.0 |
| Jona Drive | WBRT | 11 | 6 | 9 | 0.6 | 6 | 0.0 |
|  | WBT | 2087 | 3091 | 2077 | 0.2 | 2975 | 2.1 |
| Rte 7 at City Center Blvd/Countryside Blvd | SBLT | 120 | 133 | 123 | 0.3 | 137 | 0.3 |
|  | SBT | 59 | 105 | 54 | 0.7 | 100 | 0.5 |
|  | SBRT | 252 | 233 | 254 | 0.1 | 236 | 0.2 |
|  | EBLT | 203 | 343 | 205 | 0.1 | 343 | 0.0 |
|  | EBT | 2652 | 2018 | 2668 | 0.3 | 2035 | 0.4 |
|  | EBRT | 62 | 140 | 61 | 0.1 | 144 | 0.3 |
|  | NBLT | 42 | 94 | 40 | 0.3 | 89 | 0.5 |
|  | NBT | 85 | 115 | 83 | 0.2 | 115 | 0.0 |
|  | NBRT | 91 | 221 | 92 | 0.1 | 224 | 0.2 |
|  | WBLT | 53 | 247 | 52 | 0.1 | 238 | 0.6 |
|  | WBT | 1804 | 2770 | 1801 | 0.1 | 2655 | 2.2 |
|  | WBRT | 114 | 155 | 113 | 0.1 | 146 | 0.7 |
| Rte 7 at Davenport Drive | WBRT | 65 | 190 | 71 | 0.7 | 186 | 0.3 |
|  | WBT | 1905 | 3039 | 1911 | 0.1 | 2913 | 2.3 |
|  | SBRT | 66 | 133 | 65 | 0.1 | 132 | 0.1 |
| Rte 7 at Loudoun Tech Dr/Palisade Pkwy | SBLT | 83 | 180 | 83 | 0.0 | 180 | 0.0 |
|  | SBT | 49 | 87 | 50 | 0.1 | 86 | 0.1 |
|  | SBRT | 400 | 411 | 398 | 0.1 | 412 | 0.0 |
|  | EBLT | 131 | 322 | 131 | 0.0 | 325 | 0.2 |
|  | EBT | 2493 | 1937 | 2514 | 0.4 | 1957 | 0.5 |
|  | EBRT | 239 | 113 | 251 | 0.8 | 118 | 0.5 |
|  | NBLT | 49 | 273 | 50 | 0.1 | 280 | 0.4 |
|  | NBT | 19 | 96 | 17 | 0.5 | 95 | 0.1 |
|  | NBRT | 56 | 182 | 58 | 0.3 | 180 | 0.1 |
|  | WBLT | 81 | 105 | 78 | 0.3 | 98 | 0.7 |
|  | WBT | 1521 | 2545 | 1511 | 0.3 | 2409 | 2.7 |
|  | WBRT | 59 | 130 | 60 | 0.1 | 129 | 0.1 |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 EB to Cascades Pkwy NB | 148 | 220 | 153 | 0.4 | 228 | 0.5 |
|  | Rte 7 EB to Cascades Pkwy SB | 192 | 268 | 195 | 0.2 | 273 | 0.3 |
|  | Cascades Pkwy NB to Rte 7 EB | 236 | 255 | 237 | 0.1 | 254 | 0.1 |
|  | Cascades Pkwy SB to Rte 7 EB | 142 | 153 | 146 | 0.3 | 158 | 0.4 |
|  | Rte 7 WB to Cascades Pkwy NB | 130 | 252 | 124 | 0.5 | 224 | 1.8 |
|  | Rte 7 WB to Cascades Pkwy SB | 164 | 173 | 151 | 1.0 | 153 | 1.6 |


|  | Cascades Pkwy NB to Rte 7 WB | 82 | 162 | 81 | 0.1 | 163 | 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cascades Pkwy SB to Rte 7 WB | 111 | 111 | 106 | 0.5 | 107 | 0.4 |
|  | Rte 7 EB Through | 2434 | 1964 | 2359 | 1.5 | 1967 | 0.1 |
|  | Rte 7 WB Through | 1550 | 2669 | 1540 | 0.3 | 2530 | 2.7 |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SBLT | 9 | 16 | 10 | 0.3 | 17 | 0.2 |
|  | SBT | 1 | 20 | 1 | 0.0 | 21 | 0.2 |
|  | SBRT | 2 | 33 | 2 | 0.0 | 30 | 0.5 |
|  | EBLT | 99 | 53 | 96 | 0.3 | 54 | 0.1 |
|  | EBT | 2549 | 1891 | 2405 | 2.9 | 1899 | 0.2 |
|  | EBRT | 22 | 275 | 21 | 0.2 | 268 | 0.4 |
|  | NBLT | 39 | 203 | 37 | 0.3 | 200 | 0.2 |
|  | NBT | 11 | 31 | 11 | 0.0 | 30 | 0.2 |
|  | NBRT | 155 | 310 | 155 | 0.0 | 313 | 0.2 |
|  | WBLT | 60 | 236 | 62 | 0.3 | 217 | 1.3 |
|  | WBT | 1721 | 2696 | 1678 | 1.0 | 2519 | 3.5 |
|  | WBRT | 9 | 33 | 10 | 0.3 | 30 | 0.5 |
| Rte 7 at Potomac View Road | SBLT | 299 | 340 | 319 | 1.1 | 342 | 0.1 |
|  | SBT | 203 | 248 | 205 | 0.1 | 251 | 0.2 |
|  | SBRT | 216 | 190 | 214 | 0.1 | 187 | 0.2 |
|  | EBLT | 53 | 145 | 50 | 0.4 | 141 | 0.3 |
|  | EBT | 2652 | 2046 | 2498 | 3.0 | 2059 | 0.3 |
|  | EBRT | 8 | 26 | 7 | 0.4 | 27 | 0.2 |
|  | NBLT | 16 | 26 | 16 | 0.0 | 25 | 0.2 |
|  | NBT | 105 | 259 | 107 | 0.2 | 259 | 0.0 |
|  | NBRT | 353 | 445 | 337 | 0.9 | 440 | 0.2 |
|  | WBLT | 263 | 435 | 261 | 0.1 | 418 | 0.8 |
|  | WBT | 1558 | 2749 | 1521 | 0.9 | 2554 | 3.8 |
|  | WBRT | 231 | 340 | 231 | 0.0 | 316 | 1.3 |
| Rte 7 at Driveway to Mirror Ridge Shopping Center | WBRT | 43 | 70 | 41 | 0.3 | 67 | 0.4 |
|  | WBT | 2051 | 3507 | 2031 | 0.4 | 3285 | 3.8 |
|  | SBRT | 1 | 17 | 1 | 0.0 | 17 | 0.0 |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center | EBRT | 18 | 29 | 17 | 0.2 | 31 | 0.4 |
|  | EBT | 3286 | 2802 | 3118 | 3.0 | 2810 | 0.2 |
|  | NBRT | 20 | 26 | 19 | 0.2 | 25 | 0.2 |
| Rte 7 at N Sterling blvd/Cardinal Glen Circle | SBLT | 32 | 20 | 29 | 0.5 | 21 | 0.2 |
|  | SBT | 16 | 10 | 17 | 0.2 | 8 | 0.7 |
|  | SBRT | 26 | 26 | 26 | 0.0 | 26 | 0.0 |
|  | EBLT | 6 | 56 | 4 | 0.9 | 54 | 0.3 |
|  | EBT | 3064 | 2237 | 2932 | 2.4 | 2252 | 0.3 |
|  | EBRT | 236 | 535 | 222 | 0.9 | 544 | 0.4 |
|  | NBLT | 348 | 522 | 351 | 0.2 | 521 | 0.0 |
|  | NBT | 3 | 22 | 3 | 0.0 | 18 | 0.9 |
|  | NBRT | 459 | 469 | 447 | 0.6 | 463 | 0.3 |
|  | WBLT | 292 | 365 | 284 | 0.5 | 338 | 1.4 |
|  | WBT | 1720 | 3029 | 1702 | 0.4 | 2810 | 4.1 |
|  |  | 14 | 34 | 14 | 0.0 | 32 | 0.3 |
| Rte 7 at August Dr | SBLT | 357 | 148 | 362 | 0.3 | 151 | 0.2 |
|  | SBRT | 223 | 220 | 218 | 0.3 | 216 | 0.3 |
|  | EBLT | 151 | 211 | 149 | 0.2 | 213 | 0.1 |
|  | EBT | 3404 | 2515 | 3253 | 2.6 | 2522 | 0.1 |
|  | WBUT | 3 | 3 | 4 | 0.5 | 3 | 0.0 |
|  | WBT | 1803 | 3208 | 1791 | 0.3 | 2975 | 4.2 |
|  | WBRT | 155 | 144 | 161 | 0.5 | 137 | 0.6 |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church | EBRT | 39 | 16 | 42 | 0.5 | 21 | 1.2 |
|  | EBT | 3722 | 2647 | 3545 | 2.9 | 2653 | 0.1 |
|  | NBRT | 4 | 7 | 4 | 0.0 | 7 | 0.0 |
| Rte 7 at Business Dr/Cedar Dr | SBLT | 14 | 17 | 10 | 1.2 | 15 | 0.5 |
|  | SBT | 0 | 0 | 0 | 0.0 | 0 | 0.0 |
|  | SBRT | 22 | 94 | 24 | 0.4 | 94 | 0.0 |
|  | EBLT | 53 | 65 | 51 | 0.3 | 63 | 0.3 |
|  | EBT | 3669 | 2585 | 3465 | 3.4 | 2591 | 0.1 |
|  | EBRT | 4 | 4 | 4 | 0.0 | 4 | 0.0 |
|  | NBLT | 1 | 0 | 1 | 0.00 | 0 | 0.00 |


|  | NBT | 0 | 0 | 0 | 0.00 | 0 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NBRT | 0 | 3 | 0 | 0.00 | 3 | 0.00 |
|  | WBLT | 9 | 6 | 9 | 0.00 | 5 | 0.43 |
|  | WBT | 1938 | 3261 | 1928 | 0.23 | 3031 | 4.10 |
|  | WBRT | 21 | 31 | 23 | 0.43 | 30 | 0.18 |
| Rte 7 at Driveway to Chick-fil-A | EBRT1 | 26 | 15 | 23 | 0.61 | 13 | 0.53 |
|  | EBRT2 | 117 | 132 | 113 | 0.37 | 135 | 0.26 |
|  | EBT | 3657 | 2590 | 3462 | 3.27 | 2594 | 0.08 |
|  | NBRT | 7 | 25 | 6 | 0.39 | 25 | 0.00 |
| Rte 7 at Driveway to Cedar laks Plaza | WBRT | 12 | 27 | 13 | 0.28 | 25 | 0.39 |
|  | WBT | 1956 | 3262 | 1954 | 0.05 | 3035 | 4.05 |
|  | SBRT | 12 | 36 | 10 | 0.60 | 33 | 0.51 |
| Rte 7 at Community Plaza/Lakeland Drive | SBLT | 106 | 126 | 106 | 0.00 | 122 | 0.36 |
|  | SBT | 32 | 58 | 30 | 0.36 | 58 | 0.00 |
|  | SBRT | 44 | 162 | 44 | 0.00 | 166 | 0.31 |
|  | EBLT | 24 | 51 | 24 | 0.00 | 50 | 0.14 |
|  | EBT | 3423 | 2317 | 3245 | 3.08 | 2319 | 0.04 |
|  | EBRT | 100 | 115 | 95 | 0.51 | 112 | 0.28 |
|  | NBLT | 93 | 235 | 91 | 0.21 | 239 | 0.26 |
|  | NBT | 13 | 42 | 12 | 0.28 | 42 | 0.00 |
|  | NBRT | 136 | 126 | 135 | 0.09 | 122 | 0.36 |
|  | WBLT | 78 | 112 | 75 | 0.34 | 104 | 0.77 |
|  | WBT | 1831 | 2892 | 1831 | 0.00 | 2653 | 4.54 |
|  | WBRT | 47 | 157 | 48 | 0.15 | 142 | 1.23 |
| Rte 7 at Driveways right between Community Plaza and Dranesville Road | EBRT1 | 40 | 61 | 36 | 0.65 | 60 | 0.13 |
|  | EBRT2 | 28 | 34 | 25 | 0.58 | 34 | 0.00 |
|  | EBRT3 | 30 | 115 | 28 | 0.37 | 119 | 0.37 |
|  | EBT | 3625 | 2508 | 3441 | 3.10 | 2487 | 0.42 |
|  | NBRT1 | 72 | 56 | 74 | 0.23 | 58 | 0.26 |
|  | NBRT2 | 41 | 42 | 40 | 0.16 | 41 | 0.16 |
| Rte 7 at Driveways left between Community Plaza and Dranesville Road | WBRT1 | 10 | 5 | 10 | 0.00 | 4 | 0.47 |
|  | WBRT2 | 5 | 12 | 4 | 0.47 | 9 | 0.93 |
|  | WBRT3 | 15 | 24 | 17 | 0.50 | 22 | 0.42 |
|  | WBRT4 | 9 | 7 | 8 | 0.34 | 5 | 0.82 |
|  | WBRT5 | 3 | 20 | 4 | 0.53 | 18 | 0.46 |
|  | WBRT6 | 0 | 2 | 0 | 0.00 | 3 | 0.63 |
|  | WBRT7 | 6 | 3 | 6 | 0.00 | 3 | 0.00 |
|  | WBRT8 | 9 | 6 | 9 | 0.00 | 5 | 0.43 |
|  | WBRT9 | 21 | 33 | 21 | 0.00 | 30 | 0.53 |
|  | WBT | 1976 | 3149 | 1974 | 0.05 | 2906 | 4.42 |
|  | SBRT1 | 8 | 29 | 8 | 0.00 | 28 | 0.19 |
|  | SBRT2 | 2 | 8 | 2 | 0.00 | 8 | 0.00 |
|  | SBRT3 | 19 | 31 | 18 | 0.23 | 30 | 0.18 |
|  | SBRT4 | 8 | 11 | 8 | 0.00 | 11 | 0.00 |
|  | SBRT5 | 3 | 21 | 2 | 0.63 | 21 | 0.00 |
|  | SBRT6 | 0 | 3 | 0 | 0.00 | 3 | 0.00 |
|  | SBRT7 | 1 | 4 | 1 | 0.00 | 4 | 0.00 |
|  | SBRT8 | 7 | 12 | 6 | 0.39 | 12 | 0.00 |
| Rte 7 at Dranesville Rd | SBLT | 5 | 11 | 5 | 0.00 | 11 | 0.00 |
|  | SBT | 2 | 3 | 3 | 0.63 | 3 | 0.00 |
|  | SBRT | 1 | 8 | 1 | 0.00 | 8 | 0.00 |
|  | EBLT | 16 | 35 | 15 | 0.25 | 35 | 0.00 |
|  | EBT | 3371 | 2054 | 3241 | 2.26 | 2068 | 0.31 |
|  | EBRT | 293 | 368 | 270 | 1.37 | 352 | 0.84 |
|  | NBLT | 230 | 647 | 227 | 0.20 | 623 | 0.95 |
|  | NBT | 1 | 4 | 1 | 0.00 | 3 | 0.53 |
|  | NBRT | 290 | 235 | 294 | 0.23 | 236 | 0.07 |
|  | WBLT | 130 | 299 | 129 | 0.09 | 264 | 2.09 |
|  | WBT | 1755 | 2498 | 1754 | 0.02 | 2259 | 4.90 |
|  | WBRT | 9 | 17 | 9 | 0.00 | 16 | 0.25 |
| Rte 7 at Driveways right east of Dranesville Rd | EBRT | 44 | 40 | 41 | 0.46 | 40 | 0.00 |
|  | EBT | 3622 | 2260 | 3499 | 2.06 | 2275 | 0.32 |
|  | NBRT | 23 | 24 | 23 | 0.00 | 25 | 0.20 |


| Rte 7 at Fairfax County Pkwy Interchange | Rte 7 EB to Fairfax County Pkwy NB | 70 | 177 | 69 | 0.12 | 172 | 0.38 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rte 7 EB to Fairfax County Pkwy SB | 1040 | 506 | 992 | 1.51 | 509 | 0.13 |
|  | Fairfax County Pkwy NB to Rte 7 EB | 50 | 83 | 48 | 0.29 | 80 | 0.33 |
|  | Fairfax County Pkwy SB to Rte 7 EB | 609 | 191 | 614 | 0.20 | 189 | 0.15 |
|  | Rte 7 WB to Fairfax County Pkwy NB | 114 | 1076 | 112 | 0.19 | 1072 | 0.12 |
|  | Rte 7 WB to Fairfax County Pkwy SB | 129 | 164 | 127 | 0.18 | 164 | 0.00 |
|  | Fairfax County Pkwy NB to Rte 7 WB | 357 | 625 | 356 | 0.05 | 631 | 0.24 |
|  | Fairfax County Pkwy SB to Rte 7 WB | 160 | 63 | 158 | 0.16 | 66 | 0.37 |
|  | Rte 7 EB Through | 2535 | 1601 | 2424 | 2.23 | 1609 | 0.20 |
|  | Rte 7 WB Through | 1377 | 2126 | 1371 | 0.16 | 1916 | 4.67 |

## Appendix C:

VISSIM Results for Existing Conditions

|  | Model Travel Time (min) | Field Travel Time (min) | Difference <br> (\%) |
| :---: | :---: | :---: | :---: |
| Eastbound | 9.6 | 9.4 | 3\% |
| Westbound | 6.7 | 7.6 | -11\% |


| Intersection | Movement |  | Output volume (vph) | $\begin{aligned} & \text { Avg Queue } \\ & \text { (ft) } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Max Queue } \\ (\mathrm{ft}) \end{array}$ | $\begin{aligned} & \text { Storage } \\ & \text { Length (ft) } \end{aligned}$ | $\begin{gathered} \text { Delay } \\ (\mathrm{sec} / \mathrm{veh}) \end{gathered}$ | tos | Approach Delay (sec/veh) | Approach LOS | Intersection Delay (sec/veh) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Broad Run Drive (Unsignalized) | wB | RT | 18 | 0 | 0 | 300 | 0 | A | 0 | A | 0 | A |
|  |  | T | 1,650 | 0 | 0 | 5,080 | 0 | A |  |  |  |  |
|  | SB | RT | 69 | 3 | 66 | 300 | 8 | A | 8 | A |  |  |
| Jona Driveway (Unsignalized) |  | RT | 9 | 0 | 3 | 260 | 0 | A | 0 | A | 0 | A |
|  |  | T | 2,076 | 0 | 3 | 435 | 0 | A |  |  |  |  |
| Rte 7 at City Center Blva/Countryside Blvd | SB | LT | 123 | 48 | 152 | 320 | 97 | F | 47 | D | 20 | c |
|  |  | T | 54 | 48 | 152 | 945 | 92 | F |  |  |  |  |
|  |  | RT | 254 | 19 | 156 | 400 | 13 | B |  |  |  |  |
|  | EB | LT | 205 | 73 | 211 | 700 | 98 | F | 19 | B |  |  |
|  |  | T | 2,668 | 171 | 889 | 14,995 | 14 | B |  |  |  |  |
|  |  | RT | 61 | 0 | 0 | 1,445 | 1 | A |  |  |  |  |
|  | NB | LT | 40 | 33 | 109 | 405 | 100 | F | 56 | E |  |  |
|  |  | T | 83 | 33 | 109 | 700 | 97 | F |  |  |  |  |
|  |  | RT | 92 | 0 | 9 | 455 | 1 | A |  |  |  |  |
|  | WB | LT | 52 | 25 | 107 | 480 | 88 | F | 12 | B |  |  |
|  |  | T | 1,798 | 48 | 338 | 1,310 | 11 | B |  |  |  |  |
|  |  | RT | 113 | 0 | 14 | 545 | 2 | A |  |  |  |  |
| Rte 7 at Davenport Drive (Unsignalized) | wB | RT | 71 | 0 | 63 | 965 | 1 | A | 1 | A | 1 | A |
|  |  | T | 1,910 | 0 | 63 | 985 | 1 | A |  |  |  |  |
|  | SB | RT | 66 | 4 | 74 | 320 | 12 | B | 12 | B |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | LT | 83 | 39 | 117 | 345 | 101 | F | 28 | c | 17 | в |
|  |  | T | 50 | 39 | 117 | 490 | 102 | F |  |  |  |  |
|  |  | RT | 398 | 0 | 45 | 455 | 4 | A |  |  |  |  |
|  | EB | LT | 131 | 60 | 167 | 440 | 124 | F | 13 | в |  |  |
|  |  | T | 2,519 | 93 | 1,275 | 2,460 | 8 | A |  |  |  |  |
|  |  | RT | 251 | 0 | 57 | 350 | 2 | A |  |  |  |  |
|  | NB | LT | 50 | 24 | 81 | 330 | 99 | F | 54 | D |  |  |
|  |  | T | 17 | 24 | 81 | 740 | 106 | + |  |  |  |  |
|  |  | RT | 58 | 0 | 0 | 700 | 1 | A |  |  |  |  |
|  | wB | LT | 78 | 67 | 194 | 445 | 130 | F | 16 | B |  |  |
|  |  | T | 1,511 | 57 | 634 | 4,190 | 11 | B |  |  |  |  |
|  |  | RT | 60 | 0 | 0 | 690 | 1 | A |  |  |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | LT | 10 | 5 | 47 | 235 | 104 | F | 105 | F | 27 | c |
|  |  | T | 1 | 5 | 47 | 230 | 54 | D |  |  |  |  |
|  |  | RT | 2 | 1 | 25 | 230 | 130 | F |  |  |  |  |
|  | EB | LT | 96 | 67 | 224 | 330 | 118 | F | 40 | D |  |  |
|  |  | T | 2,427 | 503 | 1,122 | 4,180 | 38 | D |  |  |  |  |
|  |  | RT | 21 | 0 | 38 | 1,070 | 1 | A |  |  |  |  |
|  | NB | LT | 37 | 19 | 72 | 200 | 100 | F | 24 | c |  |  |
|  |  | T | 11 | 19 | 72 | 470 | 97 |  |  |  |  |  |
|  |  | RT | 155 | 0 | 7 | 225 | 1 | A |  |  |  |  |
|  | wB | LT | 62 | 26 | 108 | 400 | 86 | F | 8 | A |  |  |
|  |  | T | 1,678 | 29 | 286 | 950 | 5 | A |  |  |  |  |
|  |  | RT | 10 | 1 | 34 | 215 | 7 | A |  |  |  |  |
| Rte 7 at Potomac View Road | SB | LT | 320 | 111 | 402 | 590 | 93 | F | 66 | E | 39 | D |
|  |  | T | 205 | 111 | 402 | 1,260 | 78 | E |  |  |  |  |
|  |  | RT | 214 | 19 | 150 | 270 | 15 | B |  |  |  |  |
|  | EB | LT | 50 | 30 | 174 | 405 | 92 | F | 23 | c |  |  |
|  |  | T | 2,517 | 1,385 | 2,198 | 910 | 22 | c |  |  |  |  |
|  |  | RT | 7 | 1 | 63 | 840 | 6 | A |  |  |  |  |
|  | NB | LT | 16 | 217 | 675 | 175 | 99 | F | 98 | F |  |  |
|  |  | T | 107 | 217 | 675 | 455 | 90 | F |  |  |  |  |
|  |  | RT | 342 | 260 | 735 | 455 | 100 | F |  |  |  |  |
|  | wB | LT | 261 | 135 | 322 | 420 | 110 | F | 34 | c |  |  |
|  |  | T | 1,521 | 204 | 647 | 2,200 | 25 | c |  |  |  |  |
|  |  | RT | 231 | 3 | 96 | 330 | 5 | A |  |  |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping Center (Unsignalized) | wB | RT | 41 | 0 | 0 |  | 1 | A | 1 |  | 1 | A |
|  |  | T | 2,031 | 1 | 65 |  | 1 | A |  | A |  |  |
|  | EB | RT | 17 | 0 | 4 |  | 2 | A | 5 | A |  | A |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) |  | RT | 3,147 | 40 | 251 |  | 5 | A |  |  | 6 |  |
|  | NB | RT | 20 | 8 | 60 |  | 71 | F | 71 | F |  |  |
| Rte 7 at N Sterling Blvo/Cardinal Glen Circle | SB | LT | 29 | 28 | 128 | 410 | 107 | F | 73 | E | 23 | c |
|  |  | T | 17 | 28 | 128 | 410 | 116 | F |  |  |  |  |
|  |  | RT | 26 | 1 | 59 | 405 | 8 | A |  |  |  |  |
|  | EB | LT | 4 | 4 | 44 | 390 | 103 | F | 15 | в |  |  |
|  |  | T | 2,950 | 621 | 1,657 | 2,180 | 15 | B |  |  |  |  |
|  |  | RT | 224 | 5 | 117 | 395 | 4 | A |  |  |  |  |
|  | NB | LT | 351 | 78 | 224 | 300 | 95 | F | 43 | D |  |  |
|  |  | T | 3 | 78 | 224 | 550 | 82 | F |  |  |  |  |
|  |  | RT | 447 | 0 | 73 | 510 | 2 | A |  |  |  |  |
|  | wB | LT | 284 | 101 | 294 | 410 | 91 | F | 25 | c |  |  |
|  |  | T | 1,700 | 120 | 389 | 1,285 | 14 | B |  |  |  |  |
|  |  | RT | 14 | 0 | 0 | 305 | 2 | A |  |  |  |  |
| Rte 7 at Augusta Dr | SB | LT | 362 | 78 | 223 | 330 | 91 | F | 60 | E | 19 |  |
|  |  | RT | 218 | 15 | 130 | 205 | 10 | A |  |  |  |  |
|  | EB | LT | 150 3,263 | $\begin{array}{r}97 \\ 178 \\ \hline\end{array}$ | 296 1039 | 620 | 106 | F | 17 | в |  |  |
|  | wB | UT | 3,263 | 178 3 | 1,039 <br> 43 | 1,300 <br> 125 | 13 89 | B |  |  |  | B |
|  |  | T | 1,788 | 47 | 310 | 790 | 11 | B | 11 | в |  |  |
|  |  | RT | 160 | 0 | 46 | 400 | 2 | A |  |  |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | EB | RT | 42 | 67 | 416 |  | 6 | A | 12 | в | 12 |  |
|  |  | T | 3,563 | 67 | 416 |  | 12 | B |  |  |  | B |
|  | NB | RT | 4 | 2 | 32 |  | 72 | F | 72 | F |  |  |
| Rte 7 at Cedar Dr (Unsignalized) | SB | LT | 11 | 6 | 60 | 220 | 206 | F | 71 | F | 10 | A |
|  |  | T | 0 | 6 | 71 | 220 | 0 | A |  |  |  |  |
|  |  | RT | 24 | 2 | 65 | 220 | 9 | A |  |  |  |  |
|  | EB | LT | 51 | 5 | 99 | 415 | 9 | A | 14 | B |  |  |
|  |  | T | 3,486 | 261 | 923 | 800 | 14 | , |  |  |  |  |
|  |  | RT | 4 | 241 | 936 | 335 | 13 | B |  |  |  |  |
|  | NB | LT | 1 | 0 | 16 | 100 | 46 | E | 46 | E |  |  |
|  |  | T | 0 | 0 | 0 | 100 | 0 | A |  |  |  |  |
|  |  | RT | 0 | 0 | 0 | 100 | 0 | A |  |  |  |  |
|  | wB | LT | $\stackrel{9}{1,924}$ | 8 | 86 | 175 880 | 64 0 | F | 1 | A |  |  |
|  |  | RT | 1,924 | 0 | 42 | 450 | 1 | A |  |  |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | RT1 | 23 | 95 | 279 |  | 12 | B | 12 | ${ }^{\text {B }}$ |  |  |
|  |  | RT2 | 114 | 0 | 0 |  | 5 | A |  |  | 12 | B |
|  |  | T | 3,484 | 95 | 279 |  | 12 | B |  |  |  |  |
|  | NB | RT | 6 | 5 | 38 |  | 137 | F | 137 | F |  |  |
| Rte 7 at Driveway to Cedar Lake Plaza | wB | ${ }_{\text {RT }}$ | 13 | 0 | 0 |  | 1 | A | 0 | A | 0 |  |
| (Unsignalized) | SB | $\stackrel{\text { RT }}{\text { RT }}$ | $\frac{1,951}{10}$ | 0 | 0 |  | 0 | A | 0 | A |  | A |


| Intersection | Movement |  | $\left\|\begin{array}{c} \text { Output } \\ \text { volume (vph) } \end{array}\right\|$ | Avg Queue <br> (ft) | Max Queue <br> (ft) | $\begin{gathered} \text { Storage } \\ \text { Length ( } \mathrm{ft} \text { ) } \end{gathered}$ | $\begin{gathered} \text { Delay } \\ \text { (sec/veh) } \end{gathered}$ | Los | Approach Delay (sec/veh) | Approach LOS | Intersection Delay (sec/veh) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Community Plaza/Lakeland Drive | SB | LT | 106 | 50 | 175 | 370 | 99 | F | 77 | E | 13 | B |
|  |  | T | 30 | 50 | 175 | 370 | 104 | F |  |  |  |  |
|  |  | RT | 44 | 2 | 61 | 200 | 8 | A |  |  |  |  |
|  | EB | LT | 24 | 15 | 88 | 380 | 95 | F | 12 | B |  |  |
|  |  | T | 3,264 | 100 | 369 | 875 | 11 | B |  |  |  |  |
|  |  | RT | 95 | 1 | 64 | 335 | 2 | A |  |  |  |  |
|  | NB | LT | 91 | 36 | 127 | 80 | 95 | F | 44 | D |  |  |
|  |  | T | 12 | 36 | 127 | 215 | 94 | F |  |  |  |  |
|  |  | RT | 135 | 10 | 87 | 210 | 5 | A |  |  |  |  |
|  | WB | LT | 75 | 38 | 108 | 390 | 89 | F | 6 | A |  |  |
|  |  | T | 1,830 | 36 | 322 | 1,410 | 3 | A |  |  |  |  |
|  |  | RT | 48 | 1 | 91 | 1,410 | 0 | A |  |  |  |  |
| Rte 7 at NB Driveways between Community | EB | RT1 | 37 | 1 | 107 |  | 0 | A | 0 | A | 1 | A |
| Plaza and Dranesville Road (Unsignalized) |  | RT2 | 25 | 1 | 132 |  | 1 | A | 1 | A |  |  |
|  |  | RT3 | 28 | 16 | 600 |  | 1 | A | 1 | A |  |  |
|  |  | T | 3,458 | 1 | 120 |  | 1 | A | 1 | A |  |  |
|  | NB | RT1 | 74 | 0 | 41 |  |  | A | 1 | A |  |  |
|  |  | RT2 | 40 | 0 | 29 |  | 2 | A | 2 | A |  |  |
| Rte 7 at SB Driveways left between Community Plaza and Dranesville Road (Unsignalized) | wB | RT1 | 10 | 0 | 0 |  | 0 | A | 0 | A | 0 | A |
|  |  | RT2 | 4 | 0 | 4 |  | 0 | A | 0 | A |  |  |
|  |  | RT3 | 17 | 0 | 8 |  | 0 | A | 0 | A |  |  |
|  |  | RT4 | 8 | 0 | 31 |  | 0 | A | 0 | A |  |  |
|  |  | RT5 | 4 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT6 | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 6 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT8 | 9 | 0 | 6 |  | 0 | A | 0 | A |  |  |
|  |  | RT9 | 21 | 10 | 208 |  | 0 | A | 0 | A |  |  |
|  |  | T | 1,974 | 0 | 6 |  | 0 | A | 0 | A |  |  |
|  | SB | RT1 | 8 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT2 | 2 | 0 | 2 |  | 0 | A | 0 | A |  |  |
|  |  | RT3 | 18 | 0 | 9 |  | 0 | A | 0 | A |  |  |
|  |  | RT4 | 8 | 0 | 6 |  | 0 | A | 0 | A |  |  |
|  |  | RT5 | 2 | 0 | 2 |  | 0 | A |  | A |  |  |
|  |  | RT6 | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 1 | 0 | 0 |  | 0 | A |  | A |  |  |
|  |  | RT8 | 6 | 0 | 2 |  | 2 | A | 2 | A |  |  |
| Rte 7 at Dranesville Rd | SB | LT | 5 | 4 | 42 | 95 | 110 | F | 110 | F | 13 | B |
|  |  | T | 3 | 4 | 42 | 95 | 142 | F |  |  |  |  |
|  |  | RT | 1 | 7 | 66 | 95 | 11 | B |  |  |  |  |
|  | EB | LT | 15 | 9 | 60 | 590 | 115 | F | 6 | A |  |  |
|  |  | T | 3,256 | 43 | 366 | 1,390 | 6 | A |  |  |  |  |
|  |  | RT | 271 | 0 | 80 | 1,325 | 1 | A |  |  |  |  |
|  | NB | LT | 226 | 73 | 213 | 340 | 93 | F | 69 | E |  |  |
|  |  | T | 1 | 73 | 213 | 420 | 109 | F |  |  |  |  |
|  |  | RT | 294 | 38 | 176 | 415 | 51 | D |  |  |  |  |
|  | wB | LT | 129 | 55 | 140 | 420 | 119 | F | 11 | B |  |  |
|  |  | T | 1,754 | 60 | 295 | 4,350 | 3 | A |  |  |  |  |
|  |  | RT | 9 | 0 | 13 | 4,350 | 4 | A |  |  |  |  |
| Rte 7 at Driveways east of Dranesville Rd (Unsignalized) | EB | RT | 41 | 13 | 264 |  | 0 | A | 1 | A | 1 | A |
|  |  | T | 3,512 | 13 | 264 |  | 1 | A |  |  |  |  |


| Intersection/Interchange | Movement | Speed | Volume (vph) | Density (vpmpl) | Los |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Junction | 47 | 2,064 | 11 | B |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 47 | 1,977 | 14 | B |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 46 | 2,286 | 12 | B |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 55 | 3,299 | 15 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Junction | 54 | 3,102 | 14 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 48 | 2,729 | 19 | B |
|  | Rte 7 at Atlantic Blvd EB On-ramp Junction | 35 | 2,936 | 21 | c |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Junction | 41 | 1,723 | 10 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 1 | 42 | 1,609 | 13 | B |
|  | Rte 7 at Cascades Pkwy WB Weaving Segment | 42 | 1,694 | 10 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 2 | 42 | 1,542 | 12 | B |
|  | Rte 7 at Cascades Pkwy WB On-ramp Junction | 31 | 1,647 | 13 | B |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Junction | 44 | 2,668 | 15 | B |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 1 | 42 | 2,507 | 20 | C |
|  | Rte 7 at Cascades Pkwy EB Weaving Segment | 32 | 2,646 | 21 | c |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 2 | 22 | 2,401 | 37 | E |
|  | Rte 7 at Cascades Pkwy EB On-ramp Junction | 11 | 2,562 | 57 | E |


|  | Model Travel Time (min) | Field Trave Time (min) | $\begin{gathered} \hline \text { Difference } \\ (\%) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Eastbound | 7.8 | 7.5 | 4\% |
| Westbound | 9.0 | 8.2 | 9\% |


| Intersection | Movement |  | Output volume | $\begin{gathered} \text { Avg Queue } \\ \text { (ft) } \end{gathered}$ | Max Queue <br> (ft) | Storage Length (ft) | $\begin{gathered} \text { Delay } \\ \text { (sec/veh) } \end{gathered}$ | Los | Approach Delay | Approach Los | Intersection Delay ( $\mathrm{sec} / \mathrm{veh}$ ) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Broad Run Drive (Unsignalized) | wB | RT | 31 | 0 | 16 | 300 | 1 | A | 1 | A | 1 | A |
|  |  | T | 2,890 | 0 | 16 | 5,080 | 1 | A |  |  |  |  |
|  | SB | RT | 54 | 4 | 72 | 300 | 15 | B | 15 | B |  |  |
| Jona Driveway (Unsignalized) | wB | RT | 6 | 0 | 0 | 260 | 0 | A | 0 | A | 0 | A |
|  |  | T | 2,979 |  | 0 | 435 | 0 | A |  |  |  |  |
| Rte 7 at City Center Blvd/Countryside Blvd | SB | LT | 137 | 57 | 184 | 320 | 92 | F | 56 | E | 28 | c |
|  |  | T | 100 | 57 | 184 | 945 | 88 | F |  |  |  |  |
|  |  | RT | 236 | 29 | 201 | 400 | 21 | c |  |  |  |  |
|  | EB | LT | 343 | 95 | 287 | 700 | 86 | F | 27 | c |  |  |
|  |  | T | 2,034 | 94 | 563 | 14,995 | 18 | B |  |  |  |  |
|  |  | RT | 144 | 0 | 0 | 1,445 | 1 | A |  |  |  |  |
|  | NB | LT | 89 | 45 | 119 | 405 | 93 | F | 45 | D |  |  |
|  |  | T | 115 | 45 | 119 | 700 | 92 | F |  |  |  |  |
|  |  | RT | 224 | 0 | 29 | 455 | 1 | A |  |  |  |  |
|  | wB | LT | 238 | 78 | 230 | 480 | 92 | F | ${ }^{23}$ | c |  |  |
|  |  | T | 2,658 | 152 | 1,061 | 1,310 | 18 | B |  |  |  |  |
|  |  | RT | 145 | 0 | 35 | 545 | 2 | A |  |  |  |  |
| Rte 7 at Davenport Drive (Unsignalized) | wb | ${ }_{\text {RT }}$ | 187 | 2 | 259 | 965 | 2 | A | 1 | A | 2 | A |
|  |  | T | 2,909 | 2 | 259 | 985 | 1 | A |  |  |  |  |
|  | SB | ${ }_{\text {RT }}$ | 131 | 16 | 170 | 320 | 19 | c | 19 | c |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | LT | 180 | 61 | 188 | 345 | 92 | F | 37 | D | 33 | c |
|  |  | T | 86 | 61 | 188 | 490 | 90 | F |  |  |  |  |
|  |  | RT | 412 | 0 | 38 | 455 | 1 | A |  |  |  |  |
|  | EB | LT | 323 | 150 | 334 | 440 | 147 | F | 40 | D |  |  |
|  |  | T | 1,954 | 184 | 1,115 | 2,460 | 25 | c |  |  |  |  |
|  |  | ${ }_{\text {RT }}$ | 118 | 0 | 24 | 350 | 1 | A |  |  |  |  |
|  | NB | LT | 280 | 86 | 259 | 330 | 89 | F | 59 | E |  |  |
|  |  | T | 95 | 86 | 259 | 740 | 83 | F |  |  |  |  |
|  |  | RT | 180 | 0 | 0 | 700 | 1 | A |  |  |  |  |
|  | wB | LT | 98 | 98 | 291 | 445 | 148 | F | 20 | в |  |  |
|  |  | T | 2,411 | 200 | 770 | 4,190 | 15 | B |  |  |  |  |
|  |  | RT | 130 | 0 | 23 | 690 | 1 | A |  |  |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | LT | 17 | 27 | 147 | 235 | 94 | F | 93 | F | 17 | B |
|  |  | T | 21 | 27 | 147 | 230 | 89 | F |  |  |  |  |
|  |  | RT | 30 | 27 | 149 | 230 | 96 | F |  |  |  |  |
|  | EB | LT | 54 | 38 | 151 | 330 | 110 | F | 16 | B |  |  |
|  |  | T | 1,901 | 128 | 802 | 4,180 | 16 | B |  |  |  |  |
|  |  | RT | 268 | 0 | 74 | 1,070 | 2 | A |  |  |  |  |
|  | NB | LT | 200 | 64 | 193 | 200 | 96 | F | 41 | D |  |  |
|  |  | T | 30 | 64 | 193 | 470 | 84 | F |  |  |  |  |
|  |  | ${ }_{\text {RT }}$ | 313 | 7 | 104 | 225 | 1 | A |  |  |  |  |
|  | wB | LT | 216 | 89 | 250 | 400 | 116 | F | 12 | B |  |  |
|  |  | T | 2,520 | 27 | 173 | 950 | 3 | A |  |  |  |  |
|  |  | RT | 30 | 1 | 31 | 215 | 3 | A |  |  |  |  |
| Rte 7 at Potomac View Road | SB | LT | 342 | 136 | 476 | 590 | 95 | F | 74 | E | 39 | D |
|  |  | T | 251 | 136 | 476 | 1,260 | 79 | E |  |  |  |  |
|  |  | RT | 187 | 33 | 200 | 270 | 29 |  |  |  |  |  |
|  | EB | LT | 141 | 185 | 397 | 405 | 195 | F | 21 | c |  |  |
|  |  | T | 2,060 | 47 | 313 | 910 | 10 | A |  |  |  |  |
|  |  | RT | 27 | 0 | 36 | 840 | 2 | A |  |  |  |  |
|  | NB | LT | 25 | 18 | 85 | 175 | 117 | F | 79 | E |  |  |
|  |  | T | 259 | 221 | 626 | 455 | 114 | F |  |  |  |  |
|  |  | RT | 439 | 185 | 606 | 455 | 56 | E |  |  |  |  |
|  | wB | LT | 415 | 233 | 498 | 420 | 132 | F | 34 | c |  |  |
|  |  | T | 2,552 | 379 | 759 | 2,200 | 21 | c |  |  |  |  |
|  |  | RT | 316 | 5 | 140 | 330 | 5 | A |  |  |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping <br> Center (Unsignalized) | wв | ${ }_{\text {RT }}$ | ${ }^{67}$ | 0 | 4 <br> 1293 |  | 1 | A | 9 | A | 9 | A |
|  |  | T | 3,286 | 283 | 1,293 |  | 9 | A |  |  |  |  |
|  | SB | RT | 17 | 10 | 54 |  | 108 | F | 108 | F |  |  |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) | EB | ${ }_{\text {RT }}$ | 31 | 1 | 112 |  | 2 | A | 1 | A | 1 | A |
|  |  | T | 2,810 | 1 | 112 |  | 1 | A |  |  |  |  |
|  | NB | RT | 25 | 1 | 29 |  | 10 | B | 10 | B |  |  |
| Rte 7 at N Sterling Blvd/Cardinal Glen Circle | SB | LT | 21 | 15 | 88 | 410 | 99 | F | 62 | E | 32 | c |
|  |  | T | 8 | 15 | 88 | 410 | 103 |  |  |  |  |  |
|  |  | RT | 26 | 3 | 61 | 405 | 20 | B |  |  |  |  |
|  | EB | LT | 54 | 28 | 141 | 390 | 79 | E | 29 | c |  |  |
|  |  | T | 2,252 | 264 | 899 | 2,180 | 30 | c |  |  |  |  |
|  |  | RT | 544 | 68 | 456 | 395 | 18 | B |  |  |  |  |
|  | NB | LT | 521 | 99 | 292 | 300 550 | 83 | F | 45 | D |  |  |
|  |  | ${ }_{\text {RT }}$ | 18 | 99 | 292 | 550 | $\frac{81}{2}$ | F |  |  |  |  |
|  | wB | LT | 340 | 138 | 372 | 410 | 100 | F | 29 | c |  |  |
|  |  | T | 2,815 | 327 | 1,398 | 1,285 | 21 | c |  |  |  |  |
|  |  | RT | 32 | 0 | 0 | 305 | 3 | A |  |  |  |  |
| Rte 7 at Augusta Dr | SB | LT | 151 | 46 | 209 | 330 | 86 |  | 54 | D | 14 | в |
|  |  | RT | 216 | 41 | 255 | 205 | 31 | c |  |  |  |  |
|  | EB | $\stackrel{\text { LT }}{\text { T }}$ | 213 2.520 | 158 | 434 | 620 1300 | 114 | F | 10 | A |  |  |
|  | wB | UT | $\frac{2,520}{3}$ | 5 | 101 | 1,300 | 1 79 | A |  |  |  |  |
|  |  | T | 2,982 | 136 | 715 | 790 | 13 | B | 13 | в |  |  |
|  |  | RT | 138 | 0 | 29 | 400 | 2 | A |  |  |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | EB | ${ }_{\text {RT }}$ | 21 | 0 | 5 |  | 1 | A | 0 | A | 0 | A |
|  |  | T | 2,651 | 0 | 5 |  | 0 | A |  |  |  |  |
|  | NB | RT | 7 | 0 | 18 |  | 4 | A | 4 | A |  |  |
| Rte 7 at Cedar Dr (Unsignalized) | SB | LT | 15 | 1 | 53 | 220 | 14 | B | 28 | D | 3 | A |
|  |  | T | 0 | 1 | 64 | 220 | 0 | A |  |  |  |  |
|  |  | RT | 95 | 18 | 117 | 220 | 30 | D |  |  |  |  |
|  | EB | LT | 64 | 34 | 179 | 415 | 50 | E | 2 | A |  |  |
|  |  | T | 2,589 | 1 | 99 | 800 | 1 | A |  |  |  |  |
|  |  | RT | 4 |  | 105 | 335 |  | A |  |  |  |  |
|  | NB | LT | 0 | 0 | 0 | 100 | 0 | A | 8 | A |  |  |
|  |  | ${ }_{\text {T }}^{\text {RT }}$ | 0 | 0 | 0 | 100 | 0 | A |  |  |  |  |
|  | wB | RT | 3 | 1 | 16 73 | 100 175 | 8 | A |  |  |  |  |
|  |  | T | 3,035 | 24 | 474 | 880 | 2 | A | 2 | A |  |  |
|  |  | RT | 30 | 1 | 105 | 450 | 3 | A |  |  |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | RT1 | 13 |  | 213 |  |  | A | ${ }^{2}$ |  |  |  |
|  |  | RT2 | 136 | 0 | 0 |  | 2 | A |  | A | 2 | A |
|  |  | T | 2,593 | 3 | 213 |  | 2 | A |  |  |  |  |
|  | NB | RT | 25 | 1 | 38 |  | 11 | B | 11 | B |  |  |
| Rte 7 at Driveway to Cedar Lake Plaza | WB | ${ }^{\text {RT }}$ | 25 |  | 122 |  | 1 | A | 1 | A |  |  |
|  | SB | $\stackrel{\text { RT }}{ }$ | 3,038 33 | 3 | 122 |  | 1 | A | 0 | A | 1 | A |


| Intersection | Movement |  | Output <br> volume | Avg Queue (ft) | $\left\|\begin{array}{c} \text { Max Queue } \\ (\mathrm{ft}) \end{array}\right\|$ | $\begin{gathered} \text { Storage } \\ \text { Length }(\mathrm{ft}) \end{gathered}$ | $\begin{aligned} & \text { Delay } \\ & \text { (sec/veh) } \end{aligned}$ | Los | $\begin{array}{c}\text { Approach Delay } \\ \text { (sec/veh) }\end{array}$ | $\begin{aligned} & \text { Approach } \\ & \text { Los } \end{aligned}$ | $\begin{array}{\|c} \text { Intersection Delay } \\ \text { (sec/veh) } \end{array}$ | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Community Plaza/Lakeland Drive | SB | LT | 122 | 57 | 207 | 370 | 83 | F | 56 | E | 18 | B |
|  |  | T | 58 | 57 | 207 | 370 | 83 | F |  |  |  |  |
|  |  | RT | 167 | 27 | 186 | 200 | 28 | c |  |  |  |  |
|  | EB | LT | 50 | 29 | 142 | 380 | 90 | F | 20 | B |  |  |
|  |  | T | 2,319 | 117 | 367 | 875 | 19 | B |  |  |  |  |
|  |  | RT | 113 | 2 | 68 | 335 | 3 | A |  |  |  |  |
|  | NB | LT | 239 | 81 | 255 | 80 | 88 | F | 62 | E |  |  |
|  |  | T | 42 | 81 | 255 | 215 | 83 | F |  |  |  |  |
|  |  | RT | 122 | 0 | 50 | 210 | 4 | A |  |  |  |  |
|  | wB | LT | 105 | 36 | 138 | 390 | 54 | D | 5 | A |  |  |
|  |  | T | 2,657 | 1,414 | 2,303 | 1,410 | 4 | A |  |  |  |  |
|  |  | RT | 142 | 9 | 146 | 1,410 | 2 | A |  |  |  |  |
| Rte 7 at NB Driveways between Community | EB | RT1 | 60 | 0 | 113 |  | 0 | A | 0 | A | 1 | A |
| Plaza and Dranesville Road (Unsignalized) |  | RT2 | 34 | 0 | 4 |  | 1 | A | 1 | A |  |  |
|  |  | RT3 | 119 | 27 | 402 |  | 2 | A | 2 | A |  |  |
|  |  | T | 2,487 | 0 | 59 |  | 1 | A | 1 | A |  |  |
|  | NB | RT1 | 58 | 0 | 39 |  | 2 | A | 2 | A |  |  |
|  |  | RT2 | 41 | 0 | 26 |  | 3 | A | 3 | A |  |  |
| Rte 7 at SB Driveways between Community Plaza and Dranesville Road (Unsignalized) | wB | RT1 | 4 | 82 | 202 |  | 0 | A | 0 | A | 6 | A |
|  |  | RT2 | 9 | 25 | 118 |  | 0 | A | 0 | A |  |  |
|  |  | RT3 | 21 | 37 | 145 |  | 0 | A | 0 | A |  |  |
|  |  | RT4 | 5 | 32 | 123 |  | 0 | A | 0 | A |  |  |
|  |  | RT5 | 18 | 48 | 169 |  | 0 | A | 0 | A |  |  |
|  |  | RT6 | 3 | 41 | 149 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 3 | 60 | 204 |  | 0 | A | 0 | A |  |  |
|  |  | RT8 | 6 | 3,073 | 4,861 |  | 0 | A | 0 | A |  |  |
|  |  | RT9 | 30 | 87 | 245 |  | 0 | A | 0 | A |  |  |
|  |  | T | 2,911 | 46 | 159 |  | 6 | A | 6 | A |  |  |
|  | SB | RT1 | 28 | 0 | 17 |  | 0 | A | 0 | A |  |  |
|  |  | RT2 | 8 | 0 | 16 |  | 1 | A | 1 | A |  |  |
|  |  | RT3 | 30 | 0 | 22 |  | 1 | A |  | A |  |  |
|  |  | RT4 | 11 | 0 | 16 |  | 1 | A | 1 | A |  |  |
|  |  | RT5 | 21 | 0 | 20 |  | 1 | A | 1 | A |  |  |
|  |  | RT6 | 3 | 0 | 2 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 4 | 0 | 6 |  | 0 | A | 0 | A |  |  |
|  |  | RT8 | 12 | 0 | 18 |  | 4 | A | 4 | A |  |  |
| Rte 7 at Dranesville Rd | SB | LT | 11 | 9 | 76 | 95 | 107 | F | 89 | F | 46 | D |
|  |  | T | 3 | 9 | 76 | 95 | 106 | F |  |  |  |  |
|  |  | RT | 8 | 15 | 100 | 95 | 58 | E |  |  |  |  |
|  | EB | LT | 35 | 17 | 106 | 590 | 91 | F | 25 | c |  |  |
|  |  | T | 2,068 | 154 | 374 | 1,390 | 28 | c |  |  |  |  |
|  |  | RT | 353 | 0 | 30 | 1,325 | 2 | A |  |  |  |  |
|  | NB | LT | 629 | 430 | 896 | 340 | 143 | F | 110 | F |  |  |
|  |  | ${ }_{\text {T }}$ T | 4 | 430 | 896 | 420 | 103 | F |  |  |  |  |
|  |  | RT | 237 | ${ }_{61}^{61}$ | 345 <br> 1,405 | 415 | 22 | C |  |  |  |  |
|  | wB | T | 2,258 | 1,052 | 1,405 | 4,350 | 38 | D | 43 | D |  |  |
|  |  | RT | 16 | 919 | 1,457 | 4,350 | 31 | c |  |  |  |  |
| Rte 7 at Driveways east of Dranesville Rd (Unsignalized) | ${ }^{\text {EB }}$ | RT | 40 | 2 | 167 |  | 0 | A | 1 | A | 1 | A |
|  |  | T | 2,278 | 1 | 167 35 |  | 1 | A |  |  |  |  |


| Intersection /Interchange | Movement | Speed | Volume (vph) | Density (vpmpl) | tos |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Junction | 46 | 2,977 | 16 | B |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 47 | 2,838 | 20 | c |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 45 | 3,454 | 19 | B |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 53 | 3,251 | 15 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Junction | 53 | 3,06 | 14 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 48 | 2,339 | 16 | c |
|  | Rte 7 at Atlantic Blvd EB On-ramp Junction | 43 | 2,522 | 15 | B |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Junction | 41 | 2,749 | 17 | в |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 1 | 43 | 2,525 | 20 | c |
|  | Rte 7 at Cascades Pkwy WB Weaving Segment | 42 | 2,687 | 16 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 2 | 33 | 2,531 | 26 | c |
|  | Rte 7 at Cascades Pkwy WB On-ramp Junction | 18 | 2,637 | 38 | E |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Junction | 45 | 2,316 | 13 | в |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 1 | 46 | 2,086 | 15 | B |
|  | Rte 7 at Cascades Pkwy EB Weaving Segment | 42 | 2,243 | 13 | B |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 2 | 42 | 1,968 | 15 | B |
|  | Rte 7 at Cascades Pkwy EB On-ramp Junction | 32 | 2,221 | 17 | B |

## Appendix D:

## Projected 2040 Balanced Traffic Volumes



## No-Build 2040 Peak Hour Volumes



Route 7 at Davenport Dr


Route 7 at City Center Blvd \& Countryside Blvd


Route 7 at Palisade Pkwy \& Loudoun Tech Dr


## No-Build 2040 Peak Hour Volumes






## No-Build 2040 Peak Hour Volumes




## Appendix E:

VISSIM Results for 2040 No-Build Conditions
Travel Time: Rte 7 Between Rte 28 and Dranessille Rd

|  | Model Travel Time (min) |
| :--- | :---: |
| Eastbound | 15.6 |
| Westbound | 7.2 |


| Intersection | Movement |  | $\left\|\begin{array}{c} \text { Output } \\ \text { volume (vph) } \end{array}\right\|$ | Avg Queue (ft) | Max Queue (ft) | $\begin{gathered} \text { Storage } \\ \text { Length (ft) } \end{gathered}$ | $\begin{aligned} & \text { Delay } \\ & \text { (sec/veh) } \end{aligned}$ | tos | Approach Delay (sec/veh) | Approach LOS | Intersection Delay (sec/veh) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Broad Run Drive (Unsignalized) | wB | RT | 19 | 0 | 0 | 300 | 0 | A | 0 | A | 0 | A |
|  |  | T | 1,982 | 0 | 0 | 5,080 | 0 | A |  |  |  |  |
|  | ¢B | RT | 75 | 4 | 67 | 300 | 9 | A | 9 | A |  |  |
| Jona Driveway (Unsignalized) |  | RT | 10 | 0 | 0 | 260 | 0 | A | 0 | A | 0 | A |
|  |  | T | 2,465 |  | 0 | 435 | 0 | A |  |  |  |  |
| Rte 7 at City Center Blva//Countryside Blvd | SB | LT | 148 | 59 | 220 | 320 | 100 | , | 50 | D | 23 | c |
|  |  | T | 68 | 59 | 220 | 945 | 88 | F |  |  |  |  |
|  |  | RT | 305 | 32 | 235 | 400 | 17 | B |  |  |  |  |
|  | EB | LT | 234 | 77 | 230 | 700 | 93 | F | 22 | c |  |  |
|  |  | T | 2,962 | 276 | 1,315 | 14,995 | 17 | B |  |  |  |  |
|  |  | RT | 67 | 0 | 0 | 1,445 | 1 | A |  |  |  |  |
|  | NB | LT | 46 | 40 | 127 | 405 | 103 | F | 58 | E |  |  |
|  |  | T | 104 | 40 | 127 | 700 | 97 | F |  |  |  |  |
|  |  | RT | 110 | 0 | 0 | 455 | 1 | A |  |  |  |  |
|  | wB | LT | 61 | 30 | 110 | 480 | 89 | F | 15 | B |  |  |
|  |  | T | 2,132 | 78 | 513 | 1,310 | 14 | B |  |  |  |  |
|  |  | RT | 131 | 0 | 7 | 545 | 2 | A |  |  |  |  |
| Rte 7 at Davenport Drive (Unsignalized) | wB | RT | 69 | 1 | 81 | 965 | 2 | A | 1 | A | 2 | A |
|  |  | T | 2,275 | 1 | 81 | 985 | 1 | A |  |  |  |  |
|  | SB | RT | 65 | 5 | 77 | 320 | 14 | B | 14 | B |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | LT | 99 | 43 | 136 | 345 | 97 | F | 27 | c | 23 | c |
|  |  | T | 59 | 43 | 136 | 490 | 98 | F |  |  |  |  |
|  |  | RT | 489 | 0 | 80 | 455 | 4 | A |  |  |  |  |
|  | EB | LT | 139 | 57 | 169 | 440 | 114 | F | 24 | c |  |  |
|  |  | T | 2,647 | 614 | 3,190 | 2,460 | 22 | c |  |  |  |  |
|  |  | RT | 264 | 0 | 59 | 350 | 2 | A |  |  |  |  |
|  | NB | LT | 62 | 29 | 103 | 330 | 98 | , | 55 | E |  |  |
|  |  | T | 24 | 29 | 103 | 740 | 104 | + |  |  |  |  |
|  |  | RT | 71 | 0 | 0 | 700 | 1 | A |  |  |  |  |
|  | wB | LT | 91 | 72 | 218 | 445 | 121 | F | 16 | B |  |  |
|  |  | T | 1,783 | 80 | 759 | 4,190 | 12 | B |  |  |  |  |
|  |  | RT | 70 | 0 | 10 | 690 | 1 | A |  |  |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | LT | 9 | 7 | 61 | 235 | 100 | , | 103 | F | 34 | c |
|  |  | T | 5 | 7 | 61 | 230 | 109 | F |  |  |  |  |
|  |  | RT | 7 | 6 | 60 | 230 | 101 | + |  |  |  |  |
|  | EB | LT | 28 | 19 | 92 | 330 | 105 | F | 55 | E |  |  |
|  |  | T | 2,328 | 3,326 | 7,396 | 4,180 | 57 | E |  |  |  |  |
|  |  | RT | 100 | 1 | 149 | 1,070 | 5 | A |  |  |  |  |
|  | NB | LT | 47 | 22 | 78 | 200 | 99 | F | 24 | c |  |  |
|  |  | T | 12 | 22 | 78 | 470 | 97 | F |  |  |  |  |
|  |  | RT | 190 | 0 | 14 | 225 | 1 | A |  |  |  |  |
|  | wB | LT | 72 | 29 | 120 | 400 | 90 | F | 10 | A |  |  |
|  |  | T | 2,047 | 41 | 380 | 950 | 7 | A |  |  |  |  |
|  |  | RT | 10 | 0 | 31 | 215 | 6 | A |  |  |  |  |
| Rte 7 at Potomac View Road | SB | LT | 378 | 124 | 446 | 590 | 102 | F | 74 | E | 51 | D |
|  |  | T | 216 | 124 | 446 | 1,260 | 77 | E |  |  |  |  |
|  |  | RT | 262 | 47 | 246 | 270 | 29 | c |  |  |  |  |
|  | EB | LT | 49 | 28 | 145 | 405 | 85 | F | 27 | c |  |  |
|  |  | T | 2,458 | 2,043 | 2,288 | 910 | 26 | c |  |  |  |  |
|  |  | RT | 9 | 1 | 79 | 840 | 6 | A |  |  |  |  |
|  | NB | LT | 17 | 616 | 1,781 <br> 1781 | 175 | 115 | F | 171 | F |  |  |
|  |  | T | 98 | 616 | 1,781 <br> 1,828 | 455 | 94 | F |  |  |  |  |
|  | wB | LT | 314 | 3401 | $\frac{1,528}{525}$ | 452 | 209 | F | 47 | D |  |  |
|  |  | T | 1,847 | 387 | 752 | 2,200 | 27 | c |  |  |  |  |
|  |  | RT | 281 | 4 | 130 | 330 | 5 | A |  |  |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping Center (Unsignalized) | wB | RT | 43 | 0 | 0 |  | 1 | A | 6 | A | 6 | A |
|  |  | T | 2,475 | 55 | 789 |  | 6 | A |  |  |  |  |
|  | SB | RT | 5 | 0 | 21 |  | 19 | c | 19 | c |  |  |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) | EB | ${ }_{\text {RT }}$ | 15 | 381 | 1,009 |  | 4 | A | 27 | D | 29 | D |
|  |  | $\stackrel{\text { T }}{\text { RT }}$ | 3,041 <br> 13 | 381 | 1,009 |  | 28 <br> 358 | D |  |  |  |  |
|  | SB | RT | 13 | 81 | 249 | 410 | 358 | $\stackrel{\text { F }}{ }$ | 70 | E | 29 | c |
| Rte 7 at N Sterling Blvd/Cardinal Glen Circle |  | T | 16 | 25 | 128 | 410 | 106 | F |  |  |  |  |
|  |  | RT | 26 | 2 | 53 | 405 | 11 | B |  |  |  |  |
|  | EB | LT | 3 | 1 | 36 | 390 | 59 | E | 23 | c |  |  |
|  |  | T | 2,845 | 1,579 | 2,433 | 2,180 | 25 | c |  |  |  |  |
|  |  | RT | 218 | 11 | 154 | 395 | 7 | A |  |  |  |  |
|  | NB | LT | 425 | 100 | 265 | 300 | 102 | F | 46 | D |  |  |
|  |  | $\stackrel{\text { T }}{\text { RT }}$ | 4 <br> 548 | 100 | 265 | 550 510 | 131 | F |  |  |  |  |
|  |  | ${ }_{\text {RT }}^{\text {LT }}$ | 548 | 12 | 89 | 510 | 3 | A | 29 | c |  |  |
|  | wB | T | 2,087 | 175 | 685 | 1,285 | 17 | B |  |  |  |  |
|  |  | RT | 15 | 0 | 0 | 305 | 2 | A |  |  |  |  |
| Rte 7 at Augusta Dr | SB | LT | 390 | 83 | 235 | 330 | 91 | F | 62 | E | 23 | c |
|  |  | RT | 230 | 21 | 163 | 205 | 13 | B |  |  |  |  |
|  | ев | LT | 124 | 77 | 271 | 620 | 97 | F | 24 | c |  |  |
|  |  | T | 3,270 | 400 | 1,442 | 1,300 | 21 | c |  |  |  |  |
|  | wB | UT | 4 | 3 | 47 | 125 | 87 | F | 11 | в |  |  |
|  |  | T | 2,222 | 60 | 396 | 790 | 12 | B |  |  |  |  |
|  |  | RT | 160 | 0 | 52 | 400 | 2 | A |  |  |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | ев | RT | 37 | 127 | 448 |  | 8 | A | 19 | c | 19 | c |
|  |  | T | 3,582 | 127 | 448 | - | 19 | c |  |  |  |  |
|  | SB | RT | 5 | 3 | 34 |  | 128 | F | 118 | F |  |  |
| Rte 7 at Cedar Dr (Unsignalized) |  | LT | 9 | 21 | 87 | 220 | 241 | F | 81 | F | 13 | B |
|  |  | RT | 21 | 2 | 68 | 220 | 13 | B |  |  |  |  |
|  | EB | LT | 45 | 7 | 106 | 415 | 13 | , | 19 | c |  |  |
|  |  | T | 3,510 | 408 | 955 | 800 | 20 | c |  |  |  |  |
|  |  | RT | 4 | 372 | 948 | 335 | 11 | B |  |  |  |  |
|  | NB | LT | 5 | 1 | 22 | 100 | 52 | F | 52 | F |  |  |
|  |  | $\stackrel{\text { T }}{\text { RT }}$ | 0 | 0 | 0 | 100 | 0 | A |  |  |  |  |
|  | wB | LT | 11 | 11 | 86 | 175 | 87 | F | 1 | A |  |  |
|  |  | T | 2,357 | 7 | 314 | 880 | 1 | A |  |  |  |  |
|  |  | RT | 22 | 0 | 46 | 450 | 2 | A |  |  |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | RT1 | 20 | 143 | 281 |  | 13 | - | 15 | B |  |  |
|  |  | RT2 | 106 | 14 | 0 |  | ${ }^{6}$ | A |  |  | 15 | B |
|  |  | T | 3,520 | 143 | 281 |  | 15 | B |  |  |  |  |
|  | NB | ${ }_{\text {RT }}^{\text {RT }}$ | 5 | 7 | 42 53 |  | 271 | F | 271 | F |  |  |
| Rte 7 at Driveway to Cedar Lake Plaza (Unsignalized) | wB | ${ }_{\text {RT }}^{\text {T }}$ | $\stackrel{10}{2,383}$ | 1 | 53 53 |  | 1 | A | 0 | A | 0 | A |
|  | SB | RT | 8 | 0 | 0 |  | 0 | A | 0 | A |  |  |


| Intersection | Movement |  | $\left\|\begin{array}{c} \text { Output } \\ \text { volume (vph) } \end{array}\right\|$ | Avg Queue (ft) | Max Queue <br> (ft) | $\begin{gathered} \text { storage } \\ \text { Length (ft) } \end{gathered}$ | $\begin{gathered} \text { Delay } \\ \text { (sec/veh) } \end{gathered}$ | Los | Approach Delay (sec/veh) | $\begin{array}{\|c} \text { Approach } \\ \text { Los } \end{array}$ | Intersection Delay (sec/veh) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Community Plaza/Lakeland Drive | SB | LT | 115 | 55 | 172 | 370 | 102 | F | 81 | F | 13 | B |
|  |  | T | 28 | 55 | 172 | 370 | 108 | F |  |  |  |  |
|  |  | RT | 45 | 3 | 62 | 200 | 10 | A |  |  |  |  |
|  | EB | LT | 20 | 11 | 86 | 380 | 84 | F | 12 | B |  |  |
|  |  | T | 3,328 | 106 | 369 | 875 | 11 | B |  |  |  |  |
|  |  | RT | 78 | 1 | 55 | 335 | 2 | A |  |  |  |  |
|  | NB | LT | 93 | 38 | 126 | 80 | 96 | F | 44 | D |  |  |
|  |  | T | 15 | 38 | 126 | 215 | 97 | F |  |  |  |  |
|  |  | RT | 147 | 11 | 85 | 210 | 5 | A |  |  |  |  |
|  | wB | LT | 76 | 40 | 117 | 390 | 87 | F | 5 | A |  |  |
|  |  | T | 2,256 | 45 | 392 | 1,410 | 3 | A |  |  |  |  |
|  |  | RT | 46 | 1 | 84 | 1,410 | 0 | A |  |  |  |  |
| Rte 7 at Driveways right between | EB | RT1 | 36 | 1 | 115 |  | 0 | A | 0 | A | 1 | A |
| Community Plaza and Dranesville Road |  | RT2 | 24 | 1 | 223 |  | 1 | A | 1 | A |  |  |
| (Unsignalized) |  | RT3 | 29 | 17 | 637 |  | 1 | A | 1 | A |  |  |
|  |  | T | 3,544 | 1 | 169 |  | 1 | A | 1 | A |  |  |
|  | NB | RT1 | 86 | 0 | 38 |  | 1 | A | 1 | A |  |  |
|  |  | RT2 | 40 | 0 | 25 |  | 2 | A | 2 | A |  |  |
| Rte 7 at Driveways between Community Plaza and Dranesville Road (Unsignalized) | WB | RT1 | 10 | 0 | 0 |  | 0 | A | 0 | A | 0 | A |
|  |  | RT2 | 5 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT3 | 15 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT4 | 10 | 0 | 52 |  | 0 | A | 0 | A |  |  |
|  |  | RT5 | 4 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT6 | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 5 | 0 | 5 |  | 0 | A | 0 | A |  |  |
|  |  | RT8 | 11 | 0 | 80 |  | 0 | A | 0 | A |  |  |
|  |  | RT9 | 25 | 16 | 229 |  | 0 | A | 0 | A |  |  |
|  |  | T | 2,403 | 0 | 8 |  | 0 | A | 0 | A |  |  |
|  | SB | RT1 | 9 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT2 | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT3 | 20 | 0 | 18 |  | 0 | A | 0 | A |  |  |
|  |  | RT4 | 10 | 0 | 6 |  | 0 | A | 0 | A |  |  |
|  |  | RT5 | 5 | 0 |  |  | 0 | A | 0 | A |  |  |
|  |  | RT6 | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  |  | RT8 | 5 | 0 | 6 |  | 2 | A | 2 | A |  |  |
| Rte 7 at Dranesville Rd | SB | LT | 5 | 3 | 28 | 95 | 105 | F | 105 | F | 15 | B |
|  |  | T | 0 | 3 | 28 | 95 | 0 | A |  |  |  |  |
|  |  | RT | 0 | 5 | 52 | 95 | 0 | A |  |  |  |  |
|  | EB | LT | 14 | 8 | 60 | 590 | 107 | F | 6 | A |  |  |
|  |  | T | 3,341 | 45 | 366 | 1,390 | 6 | A |  |  |  |  |
|  |  | RT | 281 | 0 | 64 | 1,325 | 1 | A |  |  |  |  |
|  | NB | LT | 275 | 94 | 279 | 340 | 96 | F | 75 | E |  |  |
|  |  | T | 0 | 94 | 279 | 420 | 0 | A |  |  |  |  |
|  |  | RT | 356 | 56 | 243 | 415 | 59 | E |  |  |  |  |
|  | WB | LT | 155 | 61 | 152 | 420 | 118 | F | 11 | B |  |  |
|  |  | T | 2,132 | 70 | 388 | 4,350 | 4 | A |  |  |  |  |
|  |  | RT | 10 | 0 | 72 | 4,350 | 3 | A |  |  |  |  |
| Rte 7 at Driveways east of Dranesville Rd (Unsignalized) | ${ }^{\text {EB }}$ | RT | 36 | 12 | 243 |  | 0 | A | 1 | A | 1 | A |
|  |  | T | 3,668 | 12 | 243 |  | 1 | A |  |  |  |  |
|  |  | RT | 30 | 2 | 52 |  | 17 | c | 17 | C |  |  |


| Intersection /Interchange | Movement | Speed | Volume (vph) | Density (vpmpl) | Los |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Junction | 47 | 2,456 | 13 | B |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 47 | 2,353 | 17 | B |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 46 | 2,730 | 15 | в |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 54 | 3,692 | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Junction | 54 | 3,470 | 16 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 48 | 3,059 | 21 | B |
|  | Rte 7 at Atlantic Blvd EB On-ramp Junction | 27 | 3,283 | 30 | D |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Junction | 41 | 2,101 | 13 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 1 | 42 | 1,959 | 15 | B |
|  | Rte 7 at Cascades Pkwy WB Weaving Segment | 42 | 2,065 | 12 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 2 | 41 | 1,880 | 15 | B |
|  | Rte 7 at Cascades Pkwy WB On-ramp Junction | 28 | 1,943 | 17 | B |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Junction | 8 | 2,693 | 82 | E |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 1 | 8 | 2,489 | 101 | F |
|  | Rte 7 at Cascades Pkwy EB Weaving Segment | 7 | 2,542 | 97 | F |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 2 | 5 | 2,245 | 137 | F |
|  | Rte 7 at Cascades Pkwy EB On-ramp Junction | 5 | 2,457 | 113 | E |



| Intersection |  |  | Output volume (vph) | $\begin{gathered} \text { Avg Queue } \\ \text { (ft) } \end{gathered}$ | Max Queue <br> (ft) | Storage Length ( ft ) | $\begin{gathered} \text { Delay } \\ \text { (sec/veh) } \end{gathered}$ | Los | $\begin{array}{\|c\|} \text { Approach Delay } \\ \text { (sec/veh) } \end{array}$ | $\begin{gathered} \text { Approach } \\ \text { tos } \end{gathered}$ | $\left\lvert\, \begin{gathered} \text { Intersection Delay } \\ \text { (sec/veh) } \end{gathered}\right.$ | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Broad Run Drive (Unsignalized) | wв | RT | 29 | 0 | 36 | 300 | 1 | A | 2 | A | 2 | A |
|  |  | T | 3,269 | 0 | 36 | 5,080 | 2 | A |  |  |  |  |
|  | SB | RT | 54 | 7 | 77 | 300 | 24 | c | 24 | c |  |  |
| Jona Driveway (Unsignalized) |  | RT | 3 | 0 | 6 | 260 | 1 | A | 0 | A | 0 | A |
|  |  | T | 3,277 | 0 | 6 | 435 | 0 | A |  |  |  |  |
| Rte 7 at City Center Blvd/Countryside Blvd | SB | LT | 164 | 75 | 255 | 320 | 91 | F | 61 | E | 31 | c |
|  |  | T | 126 | 75 | 255 | 945 | 91 | F |  |  |  |  |
|  |  | RT | 287 | 53 | 273 | 400 | 30 | c |  |  |  |  |
|  | EB | LT | 380 | 104 | 311 | 700 | 86 | F | 29 | c |  |  |
|  |  | T | 2,226 | 141 | 808 | 14,995 | 21 | c |  |  |  |  |
|  |  | RT | 153 | 0 | 0 | 1,445 | 1 | A |  |  |  |  |
|  | NB | LT | 113 | 54 | 149 | 405 | 95 | F | 45 | D |  |  |
|  |  | T | 141 | 54 | 149 | 700 | 90 | F |  |  |  |  |
|  |  | RT | 271 | 0 | 5 | 455 | 1 | A |  |  |  |  |
|  | wB | LT | 256 | 81 | 245 | 480 | 88 | F | 25 | c |  |  |
|  |  | T | 2,879 | 257 | 1,631 | 1,310 | 20 | c |  |  |  |  |
|  |  | RT | 160 | 0 | 37 | 545 | 2 | A |  |  |  |  |
| Rte 7 at Davenport Drive (Unsignalized) | wB | RT | 166 | 11 | 424 | 965 | 2 | A | 2 | A | 3 | A |
|  |  | T | 3,162 | 11 | 424 | 985 | 2 | A |  |  |  |  |
|  | SB | RT | 134 | 19 | 162 | 320 | 23 | c | 23 | C |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | LT | 218 | 74 | 217 | 345 | 93 | F | 37 | D | 41 | D |
|  |  | T | 105 | 74 | 217 | 490 | 86 | F |  |  |  |  |
|  |  | RT | 499 | 0 | 64 | 455 | 2 | A |  |  |  |  |
|  | EB | LT | 349 | 270 | 462 | 440 | 231 | F | 57 | E |  |  |
|  |  | T | 2,151 | 514 | 1,934 | 2,460 | 32 | c |  |  |  |  |
|  |  | RT | 128 | 0 | 16 | 350 | 1 | A |  |  |  |  |
|  | NB | LT | 343 | 104 | 300 | 330 | 90 | F | 60 | E |  |  |
|  |  | T | 112 | 104 | 300 | 740 | 83 | F |  |  |  |  |
|  |  | RT | 221 | 0 | 0 | 700 | 1 | A |  |  |  |  |
|  | wB | LT | 104 | 103 | 315 | 445 | 144 | F | 21 | c |  |  |
|  |  | T | 2,494 | 242 | 771 | 4,190 | 17 | B |  |  |  |  |
|  |  | RT | 135 | 0 | 8 | 690 | 1 | A |  |  |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | LT | 16 | 28 | 149 | 235 | 97 | F | 94 | F | 19 | B |
|  |  | T | 21 | 28 | 149 | 230 | 97 | F |  |  |  |  |
|  |  | RT | 32 | 28 | 151 | 230 | 91 | F |  |  |  |  |
|  | EB | LT | 55 | 40 | 173 | 330 | 114 | F | 18 | B |  |  |
|  |  | T | 2,070 | 173 | 955 | 4,180 | 18 | B |  |  |  |  |
|  |  | RT | 298 | 0 | 78 | 1,070 | 2 | A |  |  |  |  |
|  | NB | LT | 251 | 79 | 235 | 200 | 98 | F | 42 | D |  |  |
|  |  | T | 28 | 79 | 235 | 470 | 87 | F |  |  |  |  |
|  |  | RT | 379 | 16 | 146 | 225 | 1 | A |  |  |  |  |
|  | wB | LT | $\begin{array}{r}227 \\ 2,596 \\ \hline\end{array}$ | 95 34 | 248 | 400 | 117 4 | F | 13 | в |  |  |
|  |  | RT | 27 | 1 | 28 | 215 | 4 | A |  |  |  |  |
| Rte 7 at Potomac View Road | SB | LT | 415 | 156 | 524 | 590 | 106 | F | 82 | F | 41 | D |
|  |  | T | 256 | 156 | 524 | 1,260 | 82 | F |  |  |  |  |
|  |  | RT | 226 | 49 | 248 | 270 | 36 | D |  |  |  |  |
|  | EB | LT | 148 | 384 | 936 | 405 | 254 | F | 27 | c |  |  |
|  |  | T | 2,272 | 137 | 808 | 910 | 13 | B |  |  |  |  |
|  |  | RT | 27 | 0 | 41 | 840 | 2 | A |  |  |  |  |
|  | NB | LT | 28 | 20 | 93 | 175 | 112 | F | 65 | E |  |  |
|  |  | $\stackrel{\text { T }}{\text { RT }}$ | 260 | 224 | 602 | 455 | 116 | F |  |  |  |  |
|  |  | RT | 542 | 67 | 311 | 455 | 38 | D |  |  |  |  |
|  | wB | LT | 420 | 228 | 517 | 420 | 125 | F | 35 | c |  |  |
|  |  | T | $\frac{2,596}{321}$ | 425 <br> 7 | 765 | $\frac{2,200}{330}$ | 24 6 | A |  |  |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping Center (Unsignalized) | wB | RT | 59 | 0 | 0 |  | 1 | A | 14 | B | 15 | c |
|  |  | T | 3,360 | 731 | 1,891 |  | 15 | B |  |  |  |  |
|  | SB | RT | 14 | 12 | 69 |  | 159 | F | 159 | F |  |  |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) | EB | RT | 34 | 23 | 583 |  | 3 | A | 2 | A | 2 | A |
|  |  | T | 3,194 | 23 | 583 |  | 2 | A |  |  |  |  |
|  | NB | RT | 25 | 2 | 37 |  | 17 | c | 17 | c |  |  |
| Rte 7 at N Sterling Blvd/Cardinal Glen Circle | SB | LT | 21 | 15 | 92 | 410 | 93 | F | 71 | E | 33 | c |
|  |  | T | 8 | 15 | 92 | 410 | 98 | F |  |  |  |  |
|  |  | RT | 25 | 5 | 70 145 | 405 390 | 44 77 | D |  |  |  |  |
|  | EB | T | 2,564 | 491 | 1,863 | 3,180 | 77 | E | 27 | c |  |  |
|  |  | RT | 629 | 95 | 530 | 395 | 21 | c |  |  |  |  |
|  | NB | LT | 637 | 118 | 366 | 300 | 88 | F | 48 | D |  |  |
|  |  | T | 16 | 118 | 366 | 550 | 79 | E |  |  |  |  |
|  |  | RT | 566 | 71 | 306 | 510 | 2 | A |  |  |  |  |
|  | wв | LT | 336 | 128 | 354 | 410 | 92 | F | 32 | c |  |  |
|  |  | T | 2,769 | 552 | 1,454 | 1,285 | 25 | c |  |  |  |  |
|  |  | RT | 28 | 0 | 0 | 305 | 2 | A |  |  |  |  |
| Rte 7 at Augusta Dr | SB | LT | 153 | 54 | 264 | 330 | 80 | F | 61 | E | 18 |  |
|  |  | RT | 228 | 63 | 310 | 205 | 47 | D |  |  |  |  |
|  | EB | LT | 2278 | 178 | 471 | 620 1300 | 117 | F | 10 | A |  |  |
|  | wB | UT | $\frac{2,918}{}$ | 10 | 177 | $\frac{1,300}{125}$ | 2 | A | 10 |  |  | в |
|  |  | T | 2,919 | 375 | 880 | 790 | 21 | c | 20 | в |  |  |
|  |  | RT | 110 | 0 | 40 | 400 | 2 | A |  |  |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | EB | RT | 19 | 2 | 176 |  | 1 | A | 1 | A | 1 | A |
|  |  | T | 3,054 | 2 | 176 |  | 1 | A |  |  |  |  |
|  | NB | RT | 5 | 0 | 23 |  | 9 | A | 9 | A |  |  |
| Rte 7 at Cedar Dr (Unsignalized) | SB | LT | 13 | 21 | 149 | 220 | 40 | E | 166 | F | 11 | B |
|  |  | T | 0 | 22 | 160 | 220 | 0 | A |  |  |  |  |
|  |  | RT | 74 | 162 | 494 | 220 | 188 | F |  |  |  |  |
|  | EB | LT | 63 | 39 | 178 | 415 | 58 | F | 3 | A |  |  |
|  |  | T | 2,991 | 17 | 610 | 800 | 2 | A |  |  |  |  |
|  |  | RT | 5 | 16 | 616 | 335 | 3 | A |  |  |  |  |
|  | NB | LT | 4 | 2 | 26 | 100 | 119 | F | 60 | F |  |  |
|  |  | RT | 5 | 0 | 20 | 100 | 13 | B |  |  |  |  |
|  | wb | LT | 3 | 1 | 72 | 175 | 32 | D | 15 | в |  |  |
|  |  | T | 3,008 | 227 | 910 | 880 | 15 | B |  |  |  |  |
|  |  | RT | 25 | 33 | 407 | 450 | 10 | B |  |  |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | RT1 | 16 | 10 | 270 |  | 3 | A | 4 | A | 5 | A |
|  |  | RT2 | 148 | 0 | 0 |  | 6 | A |  |  |  |  |
|  |  | T | 2,988 | 10 | 270 |  | 4 | A |  |  |  |  |
|  | NB | RT | 25 | 9 | 83 |  | 62 | F | 62 | F |  |  |
| Rte 7 at Driveway to Cedar Lake Plaza | wB | RT | 18 | 59 | 408 |  | 1 | A | 8 | A | 8 |  |
| (Unsignalized) | SB | T <br> RT | 3,028 32 | 59 | 408 0 |  | 8 | A | 1 | A |  | A |


| Intersection | Movement |  | Output volume | Avg Queue (ft) | Max Queue <br> (ft) | $\begin{gathered} \text { Storage } \\ \text { Length }(\mathrm{tt}) \end{gathered}$ | $\begin{gathered} \text { Delay } \\ \text { (sec/veh) } \end{gathered}$ | Los | $\begin{array}{\|c\|} \text { Approach Delay } \\ \text { (sec/veh) } \end{array}$ | $\begin{aligned} & \text { Approach } \\ & \text { Los } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Intersection Delay } \\ \text { (sec/veh) } \end{array}$ | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Community Plaza/Lakeland Drive | SB | LT | 131 | 70 | 222 | 370 | 84 | F | 65 | E | 20 | B |
|  |  | T | 60 | 70 | 222 | 370 | 85 |  |  |  |  |  |
|  |  | RT | 174 | 46 | 217 | 200 | 44 | D |  |  |  |  |
|  | EB | LT | 48 | 27 | 140 | 380 | 89 | F | 20 | B |  |  |
|  |  | T | 2,703 | 142 | 373 | 875 | 19 | B |  |  |  |  |
|  |  | RT | 107 | 2 | 73 | 335 | 3 | A |  |  |  |  |
|  | NB | LT | 262 | 85 | 262 | 80 | 86 | F | 62 | E |  |  |
|  |  | T | 40 | 85 | 262 | 215 | 91 | F |  |  |  |  |
|  |  | RT | 133 | 1 | 54 | 210 | 4 | A |  |  |  |  |
|  | wB | LT | 78 | 27 | 118 | 390 | 62 | E | 7 | A |  |  |
|  |  | T | 2,611 | 1,924 | 2,669 | 1,410 | 6 | A |  |  |  |  |
|  |  | RT | 111 | 6 | 131 | 1,410 | 1 | A |  |  |  |  |
| Rte 7 at Driveways right between | EB | RT1 | 74 | 1 | 137 |  | 0 | A | 0 | A | 1 | A |
| Community Plaza and Dranesville Road |  | RT2 | 41 | 3 | 156 |  | 2 | A | 2 | A |  |  |
| (Unsignalized) |  | RT3 | 135 | 71 | 606 |  | 2 | A | 2 | A |  |  |
|  |  | T | 2,873 | 2 | 146 |  | 1 | A | 1 | A |  |  |
|  | NB | RT1 | 66 | 0 | 36 |  | 2 | A | 2 | A |  |  |
|  |  | RT2 | 45 | 0 | 33 |  | 3 | A | 3 | A |  |  |
| Rte 7 at Driveways between Community Plaza and Dranesville Road (Unsignalized) | wB | RT1 | 4 | 93 | 208 |  | 0 | A | 0 | A | 7 | A |
|  |  | RT2 | 9 | 30 | 113 |  | 0 | A | 0 | A |  |  |
|  |  | RT3 | 20 | 43 | 146 |  | 0 | A | 0 | A |  |  |
|  |  | RT4 | 4 | 36 | 127 |  | 0 | A | 0 | A |  |  |
|  |  | RT5 | 15 | 53 | 169 |  | 0 | A | 0 | A |  |  |
|  |  | RT6 | 0 | 45 | 143 |  | 0 | A | 0 | A |  |  |
|  |  | RT7 | 3 | 69 | 206 |  | 0 | A | 0 | A |  |  |
|  |  | RT8 | 5 | 6,345 | 7,494 |  | 0 | A | 0 | A |  |  |
|  |  | RT9 | 31 | 95 | 247 |  | 0 | A | 0 | A |  |  |
|  |  | T | 2,793 | 53 | 159 |  | 7 | A | 7 | A |  |  |
|  | SB | RT1 | 29 | 0 | 13 |  | 0 | A | 0 | A |  |  |
|  |  | RT2 | 10 | 0 | 18 |  | 1 | A | 1 | A |  |  |
|  |  | RT3 | 34 | 0 | 27 |  | 1 | A | 1 | A |  |  |
|  |  | RT4 | 10 | 0 | 10 |  | 1 | A | 1 | A |  |  |
|  |  | RT5 | 25 | 0 | 22 |  | 1 | A | 1 | A |  |  |
|  |  | RT6 | 5 | 0 | 14 |  | 1 | A | 1 | A |  |  |
|  |  | RT7 | 5 | 0 | 11 |  | 1 | A | 1 | A |  |  |
|  |  | RT8 | 10 | 0 | 21 |  | 5 | A | 5 | A |  |  |
| Rte 7 at Dranesville Rd | SB | LT | 10 | 9 | 88 | 95 | 95 | F | 85 | F | 59 | E |
|  |  | T | 5 | 9 | 88 | 95 | 101 | F |  |  |  |  |
|  |  | RT | 11 | 15 | 112 | 95 | 68 | E |  |  |  |  |
|  | EB | LT | 34 | 15 | 94 | 590 | 84 | F | 23 | c |  |  |
|  |  | T | 2,405 | 165 | 372 | 1,390 | 26 | c |  |  |  |  |
|  |  | RT | 408 | 1 | 68 | 1,325 | 3 | A |  |  |  |  |
|  | NB | LT | 626 | 1,010 | 1,217 | 340 | 230 | F | 201 | F |  |  |
|  |  | ${ }_{\text {T }}^{\text {RT }}$ | 4 | 1,010 | 1,217 | 420 | 300 | F |  |  |  |  |
|  |  | RT | 239 | 796 | 1,209 | 415 | 124 | F |  |  |  |  |
|  | wB | T | 2,134 | 1,179 | 1,404 | 4,350 | 44 | D | 49 | D |  |  |
|  |  | RT | 11 | 1,071 | 1,455 | 4,350 | 38 | D |  |  |  |  |
| Rte 7 at Driveways east of Dranesville Rd (Unsignalized) | ${ }_{\text {EB }}$ | RT | 40 | 4 | 240 |  | 0 | A | 1 | A | 1 | A |
|  |  | T | 2,617 | 4 | 240 |  | 1 | A |  |  |  |  |
|  |  | RT | 30 | 1 | 48 |  | 9 | A | 9 | A |  |  |


| Intersection /Interchange | Movement | Speed | Volume (vph) | Density (vpmpl) | Los |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Junction | 46 | 3,279 | 18 | B |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 47 | 3,124 | 22 | c |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 44 | 3,868 | 22 | c |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 54 | 3,648 | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Junction | 53 | 3,420 | 16 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 48 | 2,535 | 18 | c |
|  | Rte 7 at Atlantic Blvd EB On-ramp Junction | 37 | 2,759 | 19 | B |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Junction | 41 | 2,880 | 18 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 1 | 43 | 2,648 | 21 | c |
|  | Rte 7 at Cascades Pkwy WB Weaving Segment | 41 | 2,847 | 17 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment 2 | 30 | 2,682 | 30 | D |
|  | Rte 7 at Cascades Pkwy WB On-ramp Junction | 16 | 2,737 | 44 | E |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Junction | 45 | 2,596 | 15 | в |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 1 | 46 | 2,343 | 17 | в |
|  | Rte 7 at Cascades Pkwy EB Weaving Segment | 42 | 2,423 | 15 | B |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment 2 | 42 | 2,121 | 17 | B |
|  | Rte 7 at Cascades Pkwy EB On-ramp Junction | 27 | 2,428 | 23 | c |

## Appendix F: <br> VDOT Junction Screening Tool (vJuST) Evaluation Summary

Route 7 Concept Study
JuST Analysis of Potential Intersection Configuration Options

| Intersection Type | Comments |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Route 7 @ City Center / Countryside Blvd | Route 7 @ Loudoun Tech Dr | Route 7 @ <br> Campus Dr | Route 7 @ <br> Potomac View Rd | Route 7 @ Cardinal Glen Cir | Route 7 @ Cedar Dr | Route 7 @ Dranesville Rd | Route 7 @ <br> Lakeland Dr |
| Conventional |  |  |  |  |  |  |  |  |
| Bowtie | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Center Turn Overpass |  |  |  |  |  |  |  |  |
| Continuous Green T | Design for 3-leg Int | Design for 3-leg Int | Design for 3-leg Int | Design for 3-leg Int | Design for 3-leg Int | Design for 3-leg Int | Design for 3-leg Int | Design for 3-leg Int |
| Echelon |  |  |  |  |  |  |  |  |
| Full Displaced Left Turn | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Median U Turn | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Partial Displaced Left Turn | Not enough Space |  |  |  |  |  |  |  |
| Partial Median U Turn | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Quadrant Roadway | Analyzed only for S-W Quad due to space | Not enough Space | Not enough Space | Analyzed only for N-W Quad due to space | Analyzed only for N-E Quad due to space | Not enough Space | Not enough Space | Not enough Space |
| Restricted Crossing UTurn (RCUT) / Superstreet | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Single Loop | Analyzed only for S-W Quad due to space | Not enough Space | Not enough Space | Analyzed only for N-W Quad due to space | Analyzed only for N-E Quad due to space | Not enough Space | Not enough Space | Not enough Space |
| Split Intersection | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Roundabout | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume |
| Two Way Stop Control | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume |
| Traditional Diamond | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Contraflow Left | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Displaced Left Turn | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Diverging Diamond | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Double Roundabout | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Michigan Urban Diamond |  |  |  |  |  |  |  |  |
| Partial Cloverleaf | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space | Not enough Space |
| Single Point |  |  |  |  |  |  |  |  |
| Single Roundabout | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume | Too high of Volume |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options

## Route 7 at City Center Blvd / Countryside Blvd

| 1 | Conventional | - | Y |  |  |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |  |  |  |  |  |  |
| 3 | Center Turn Overpass | Link | Y |  |  |  |  |  |  |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |  |  |  |  |  |  |
| 5 | Echelon | Link | Y |  |  |  |  |  |  |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |  |  |
| 8 | Partial Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |  |  |
| 10 | Quadrant Roadway N-E | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 13 | Quadrant Roadway S-W | Link | Y |  |  |  |  |  |  |  |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |  |  |
| 15 | Single Loop | Link | Y |  |  |  |  |  |  |  |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |  |  |  |  |  |  |
| Unsignalized Intersections |  |  |  |  |  |  |  |  |  |  |
| 17 | 50 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |  |
| 18 | 75 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |  |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |  |
| 20 | Two-Way Stop Control | - | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |  |
| \# | Interchanges | Information | Consider? |  |  |  |  |  |  |  |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 26 | Michigan Urban Diamond | Link | Y |  |  |  |  |  |  |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |  |  |  |  |  |  |
| 28 | Single Point | Link | Y |  |  |  |  |  |  |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |  |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

AM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \mathrm{V} / \mathrm{C} \end{gathered}$ | Accommodation <br> Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.87 |  | 48 |  |
| Center Turn Overpass | - | 0.72 | + | 32 |  |
| Echelon | - | 0.74 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.77 | - | 44 |  |
| Quadrant Roadway | S-W | 0.83 |  | 40 |  |
| Single Loop | - | 0.83 | - | 28 |  |
| Contraflow Left | - | 0.35 |  | 32 | Freeway direction is EB-WB |
| Displaced Left Turn | - | 0.25 | - | 28 | Freeway direction is EB-WB |
| Double Roundabout | - | 0.32 | + | 16 | Freeway direction is EB-WB |
| Michigan Urban Diamond | - | 0.31 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.22 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | Maximum V/C | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.96 |  | 48 |  |
| Center Turn Overpass | - | 0.76 | + | 32 |  |
| Echelon | - | 0.79 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.88 | - | 44 |  |
| Quadrant Roadway | S-W | 0.95 |  | 40 |  |
| Single Loop | - | 0.85 | - | 28 |  |
| Contraflow Left | - | 0.39 |  | 32 | Freeway direction is EB-WB |
| Displaced Left Turn | - | 0.34 | - | 28 | Freeway direction is EB-WB |
| Double Roundabout | - | 0.79 | + | 16 | Freeway direction is EB-WB |
| Michigan Urban Diamond | - | 0.39 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.32 | - | 32 | Freeway direction is EB-WB |

Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

Route 7 at Loudoun Tech Dr

| 1 | Conventional | - | Y |  |
| :---: | :---: | :---: | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |
| 3 | Center Turn Overpass | Link | Y |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |
| 5 | Echelon | Link | Y |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |
| 8 | Partial Displaced Left Turn | Link | Y |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |
| 10 | Quadrant Roadway N-E | Link | N | Right-of-way restrictions identified |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |
| 13 | Quadrant Roadway S-W | Link | N | Right-of-way restrictions identified |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |
| 15 | Single Loop | Link | N | Right-of-way restrictions identified |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |
| Unsignalized Intersections |  |  |  |  |
| 17 | 50 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |
| 18 | 75 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |
| 20 | Two-Way Stop Control | - | N | Unable to accommodate magnitude of traffic volumes |
| \# | Interchanges | Information | Consider? | Justification |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |
| 26 | Michigan Urban Diamond | Link | Y |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |
| 28 | Single Point | Link | Y |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

| AM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Results |  |  |  |  |  |
|  |  |  |  |  |  |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \mathrm{V} / \mathrm{C} \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.76 |  | 48 |  |
| Center Turn Overpass | - | 0.66 | + | 32 |  |
| Echelon | - | 0.71 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.73 | - | 44 |  |
| Michigan Urban Diamond | - | 0.28 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.32 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation <br> Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.97 |  | 48 |  |
| Center Turn Overpass | - | 0.73 | + | 32 |  |
| Echelon | - | 0.76 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.85 | - | 44 |  |
| Michigan Urban Diamond | - | 0.57 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.44 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

Route 7 at Potomac View Rd

| 1 | Conventional | - | Y |  |  |  |
| :---: | :--- | :---: | :---: | :--- | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |  |  |
| 3 | Center Turn Overpass | Link | Y |  |  |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |  |  |
| 5 | Echelon | Link | Y |  |  |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 8 | Partial Displaced Left Turn | Link | Y |  |  |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 10 | Quadrant Roadway N-E | Link | N | Right-of-way restrictions identified |  |  |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |  |  |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |  |  |
| 13 | Quadrant Roadway S-W | Link | N | Right-of-way restrictions identified |  |  |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 15 | Single Loop | Link | N | Right-of-way restrictions identified |  |  |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |  |  |
|  |  |  |  |  |  |  |
| 17 | Unsignalized Intersections |  |  |  |  |  |
| 18 | Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 20 | Two-Way Stop Control | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| \# | Interchanges | - | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |  |  |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |  |  |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |  |  |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |  |  |
| 26 | Michigan Urban Diamond | Link | Y |  |  |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |  |  |
| 28 | Single Point | Link | Y |  |  |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

AM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | Maximum V/C | Accommodation <br> Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 1.17 |  | 48 |  |
| Center Turn Overpass | - | 0.76 | + | 32 |  |
| Echelon | - | 0.82 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.88 | - | 44 |  |
| Michigan Urban Diamond | - | 0.49 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.48 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $50^{e^{x}}$ | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \mathrm{V} / \mathrm{C} \end{gathered}$ | Accommodation <br> Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 1.18 | ¢ | 48 |  |
| Center Turn Overpass | - | 0.79 | $+$ | 32 |  |
| Echelon | - | 0.87 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.91 | - | 44 |  |
| Michigan Urban Diamond | - | 0.65 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.58 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

Route 7 at Cardinal Glen Circle

| 1 | Conventional | - | Y |  |  |  |
| :---: | :--- | :---: | :---: | :--- | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |  |  |
| 3 | Center Turn Overpass | Link | Y |  |  |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |  |  |
| 5 | Echelon | Link | Y |  |  |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 8 | Partial Displaced Left Turn | Link | Y |  |  |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 10 | Quadrant Roadway N-E | Link | Y |  |  |  |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |  |  |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |  |  |
| 13 | Quadrant Roadway S-W | Link | N | Right-of-way restrictions identified |  |  |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 15 | Single Loop | Link | Y |  |  |  |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |  |  |
|  |  |  |  |  |  |  |
| 17 | Unsignalized Intersections |  |  |  |  |  |
| 18 | Mini Roundabout | Link Roundabout | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 20 | Two-Way Stop Control | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| \# | Interchanges | - | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |  |  |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |  |  |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |  |  |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |  |  |
| 26 | Michigan Urban Diamond | Link | Y |  |  |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |  |  |
| 28 | Single Point | Link | Y |  |  |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

| AM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Results |  |  |  |  |  |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.97 | ¢ $¢$ ¢ | 48 |  |
| Center Turn Overpass | - | 0.72 | $+$ | 32 |  |
| Echelon | - | 0.73 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.73 | - | 44 |  |
| Michigan Urban Diamond | - | 0.05 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.05 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.97 |  | 48 |  |
| Center Turn Overpass | - | 0.78 | + | 32 |  |
| Echelon | - | 0.92 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.95 | - | 44 |  |
| Michigan Urban Diamond | - | 0.61 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.78 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

## Route 7 at Cedar Drive

| 1 | Conventional | - | Y |  |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |  |  |  |  |  |
| 3 | Center Turn Overpass | Link | Y |  |  |  |  |  |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |  |  |  |  |  |
| 5 | Echelon | Link | Y |  |  |  |  |  |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |  |
| 8 | Partial Displaced Left Turn | Link | Y |  |  |  |  |  |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |  |
| 10 | Quadrant Roadway N-E | Link | Y |  |  |  |  |  |  |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 13 | Quadrant Roadway S-W | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |  |
| 15 | Single Loop | Link | Y |  |  |  |  |  |  |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |  |  |  |  |  |
| Unsignalized Intersections |  |  |  |  |  |  |  |  |  |
| 17 | 50 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |
| 18 | 75 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |
| 20 | Two-Way Stop Control | - | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |
| \# | Interchanges | Information | Consider? |  |  |  |  |  |  |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 26 | Michigan Urban Diamond | Link | Y |  |  |  |  |  |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |  |  |  |  |  |
| 28 | Single Point | Link | Y |  |  |  |  |  |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |  |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

| AM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Results |  |  |  |  |  |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.97 |  | 48 |  |
| Center Turn Overpass | - | 0.72 | $+$ | 32 |  |
| Echelon | - | 0.73 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.73 | - | 44 |  |
| Quadrant Roadway | N-E | 0.99 |  | 40 |  |
| Single Loop | - | 0.97 | - | 28 |  |
| Michigan Urban Diamond | - | 0.05 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.05 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | Maximum V/C | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.71 | ¢ | 48 |  |
| Center Turn Overpass | - | 0.64 | + | 32 |  |
| Echelon | - | 0.64 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.68 | - | 44 |  |
| Quadrant Roadway | N-E | 0.92 |  | 40 |  |
| Single Loop | - | 0.88 | - | 28 |  |
| Michigan Urban Diamond | - | 0.06 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.06 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

Route 7 at Dranesville Rd

| 1 | Conventional | - | Y |  |  |  |
| :---: | :--- | :---: | :---: | :--- | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |  |  |
| 3 | Center Turn Overpass | Link | Y |  |  |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |  |  |
| 5 | Echelon | Link | Y |  |  |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 8 | Partial Displaced Left Turn | Link | Y |  |  |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 10 | Quadrant Roadway N-E | Link | N | Right-of-way restrictions identified |  |  |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |  |  |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |  |  |
| 13 | Quadrant Roadway S-W | Link | N | Right-of-way restrictions identified |  |  |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |  |  |
| 15 | Single Loop | Link | N | Right-of-way restrictions identified |  |  |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |  |  |
|  |  |  |  |  |  |  |
| 17 | Unsignalized Intersections | Mini Roundabout | Link | N |  |  |
| 18 | 75 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |
| 20 | Two-Way Stop Control | - | N | Unable to accommodate magnitude of traffic volumes |  |  |
| $\#$ | Interchanges | Information | Consider? |  |  |  |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |  |  |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |  |  |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |  |  |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |  |  |
| 26 | Michigan Urban Diamond | Link | Y |  |  |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |  |  |
| 28 | Single Point | Link | Y |  |  |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

AM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 1.07 |  | 48 |  |
| Center Turn Overpass | - | 0.66 | + | 32 |  |
| Echelon | - | 0.66 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.72 | - | 44 |  |
| Michigan Urban Diamond | - | 0.30 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.39 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \mathrm{V} / \mathrm{C} \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 1.01 | ¢ $<$ ¢ | 48 |  |
| Center Turn Overpass | - | 0.82 | + | 32 |  |
| Echelon | - | 0.84 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.75 | - | 44 |  |
| Michigan Urban Diamond | - | 0.78 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.82 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

## vJuST Analysis of Potential Intersection Configuration Options

## Route 7 at Lakeland Drive

| 1 | Conventional | - | Y |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: |
| 2 | Bowtie | Link | N | Insufficient intersection spacing |  |  |  |  |
| 3 | Center Turn Overpass | Link | Y |  |  |  |  |  |
| 4 | Continuous Green-T | Link | N | Not feasible for roadway facility type |  |  |  |  |
| 5 | Echelon | Link | Y |  |  |  |  |  |
| 6 | Full Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 7 | Median U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |
| 8 | Partial Displaced Left Turn | Link | Y |  |  |  |  |  |
| 9 | Partial Median U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |
| 10 | Quadrant Roadway N-E | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 11 | Quadrant Roadway N-W | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 12 | Quadrant Roadway S-E | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 13 | Quadrant Roadway S-W | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 14 | Restricted Crossing U-Turn | Link | N | Insufficient intersection spacing |  |  |  |  |
| 15 | Single Loop | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 16 | Split Intersection | Link | N | Insufficient intersection spacing |  |  |  |  |
| Unsignalized Intersections |  |  |  |  |  |  |  |  |
| 17 | 50 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |
| 18 | 75 Mini Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |
| 19 | Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |
| 20 | Two-Way Stop Control | - | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |
| $\#$ | Interchanges | Information | Consider? |  |  |  |  |  |
| 21 | Traditional Diamond | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 22 | Contraflow Left | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 23 | Displaced Left Turn | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 24 | Diverging Diamond | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 25 | Double Roundabout | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 26 | Michigan Urban Diamond | Link | Y |  |  |  |  |  |
| 27 | Partial Cloverleaf | Link | N | Right-of-way restrictions identified |  |  |  |  |
| 28 | Single Point | Link | Y |  |  |  |  |  |
| 29 | Single Roundabout | Link | N | Unable to accommodate magnitude of traffic volumes |  |  |  |  |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options

The results of the vJuST analysis for the AM and PM peak scenarios are shown below. Overall the interchange options provide the greatest improvement from the current conventional intersection. The Center Turn Overpass and the Echelon provide the best improvements for non-interchange options.

| AM Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Results |  |  |  |  |  |
|  |  |  |  | $c 0^{e^{x}}$ | Notes |
| Type | Dir | Maximum V/C | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 1.01 | ¢ $\square_{\text {¢ }}$ | 48 |  |
| Center Turn Overpass | - | 0.70 | + | 32 |  |
| Echelon | - | 0.72 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.77 | - | 44 |  |
| Michigan Urban Diamond | - | 0.17 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.15 | - | 32 | Freeway direction is EB-WB |

## Route 7 Concept Study

vJuST Analysis of Potential Intersection Configuration Options
PM Peak Hour

| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation <br> Compared to Conventional | Weighted Total Conflict Points |  |
| Conventional | - | 0.95 |  | 48 |  |
| Center Turn Overpass | - | 0.61 | + | 32 |  |
| Echelon | - | 0.70 | + | 28 | NB shares approach with WB |
| Partial Displaced Left Turn | - | 0.74 | - | 44 |  |
| Michigan Urban Diamond | - | 0.25 | + | 24 | Freeway direction is EB-WB |
| Single Point | - | 0.24 | - | 32 | Freeway direction is EB-WB |

## Appendix G:

VISSIM Results for 2040 Build Alternative 1 Conditions

| Travel Time: Rte 7 Between Rte 28 and Dranesville Rd |
| :--- |
|  |


| Intersection | Movement |  | $\left\|\begin{array}{c} \text { Output } \\ \text { volume (vph) } \end{array}\right\|$ | Avg Queue <br> (ft) | Max Queue <br> (ft) | Storage Length (ft) | $\begin{gathered} \text { Delay } \\ \text { (sec/veh) } \end{gathered}$ | Los | Approach Delay (sec/veh) | Approach Los | Intersection Delay (sec/veh) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Broad Run Drive (Unsignalized) | WB | RT | 19 | 0 | 0 | 300 | 0 | A | 1 | A | 1 | A |
|  |  | T | 1,981 | 0 | 0 | 5,080 | 1 | A |  |  |  |  |
|  | SB | RT | 75 | 4 | 66 | 300 | 10 | A | 10 | A |  |  |
| Jona Driveway (Unsignalized) |  | RT | 10 | 0 | 8 | 260 | 1 | A | 1 | A | 1 | A |
|  |  | T | 2,678 | 0 | 8 | 435 | 1 | A |  |  |  |  |
| Rte 7 at City Center Blva/Countryside Blvd | SB | RT | 218 | 81 | 385 | 400 | 64 | E | 64 | E | 27 | c |
|  | EB | LT | 235 | 217 | 1,005 | 700 | 91 | F | 25 | c |  |  |
|  |  | T | 3,126 | 217 | 1,005 | 14,995 | 21 | c |  |  |  |  |
|  |  | RT | 134 | 0 | 14 | 1,445 | 5 | A |  |  |  |  |
|  | NB | RT | 259 | 48 | 211 | 455 | 87 | F | 87 | F |  |  |
|  | WB | LT | 61 | 106 | 686 | 480 | 72 | E | 20 | c |  |  |
|  |  | T | 2,164 | 106 | 686 | 1,310 | 19 | B |  |  |  |  |
|  |  | RT | 236 | 12 | 182 | 545 | 19 | B |  |  |  |  |
| Rte 7 at Davenport Drive | wB | RT | 67 | 186 | 892 | 965 | 8 | A | 21 | c | 33 | c |
|  |  | T | 2,241 | 186 | 892 | 985 | 21 | c |  |  |  |  |
|  |  | UT | 160 | 186 | 892 | 900 | 58 | E |  |  |  |  |
|  | SB | T | 3,238 | 465 | 1,440 | 1,300 | 38 | D | 39 | D |  |  |
|  |  | UT | 150 | 465 | 1,440 | 800 | 67 | E |  |  |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | RT | 159 | 41 | 168 | 530 | 69 | E | 69 | E | 22 | c |
|  | EB | LT | 148 | 121 | 516 | 440 | 71 | E | 18 | в |  |  |
|  |  | T | 2,908 | 121 | 516 | 2,460 | 16 | B |  |  |  |  |
|  |  | RT | 337 | 0 | 91 | 350 | 5 | A |  |  |  |  |
|  | NB | RT | 70 | 18 | 86 | 700 | 68 | E | 68 | E |  |  |
|  | wB | LT | 93 | 149 | 700 | 530 | 140 | F | 24 | c |  |  |
|  |  | T | 1,813 | 149 | 700 | 4,190 | 19 | B |  |  |  |  |
|  |  | RT | 93 | 1 | 115 | 690 | 4 | A |  |  |  |  |
| Cascades Pkwy at EB Ramps to/from Route 7 | SB | T | 1,389 | 88 | 252 | 400 | 8 | A | 16 | в | 16 | B |
|  |  | LT | 193 | 88 | 252 | 275 | 69 | E | 14 |  |  |  |
|  | EB | $\frac{\text { LT }}{\text { RT }}$ | 307 165 | 24 | 161 | 900 350 | 21 | C |  | в |  |  |
|  |  | T | 1,180 | 54 | 263 | 1,000 | 19 | B | 16 |  |  |  |
|  | NB | RT | 279 | 54 | 263 | 1,000 | 3 | A |  | B |  |  |
| Cascades Pkwy at WB Ramps to/from Route 7 | SB | RT | 133 | 69 | 378 | 1,000 | 1 | A | 19 | в | 15 | в |
|  |  | T | 1,382 | 69 | 378 | 1,000 | 21 | c |  |  |  |  |
|  | WB | LT | 196 | 31 | 233 | 800 | 25 | C | 15 | в |  |  |
|  | NB | T | 1,304 | 34 | 191 | 400 | 7 | A | 10 | A |  |  |
|  | NB | LT | 186 | 34 | 191 | 400 | 28 | c |  |  |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | RT | 20 | 1 | 38 | 230 | 10 | A | 10 | A | 80 | E |
|  | EB | LT | 31 | 742 | 1,569 | 425 | 136 | F | 85 | F |  |  |
|  |  | T | 2,630 | 742 | 1,569 | 4,180 | 88 | F |  |  |  |  |
|  |  | RT | 124 | 0 | 0 | 1,070 | 14 | B |  |  |  |  |
|  | NB | RT | 198 | 317 | 607 | 500 | 393 | F | 393 | F |  |  |
|  | wB | T | 2,008 | 479 | 1,012 | 950 | 7 | A | 50 | D |  |  |
|  |  | ${ }^{\text {RT }}$ | 19 | 479 | 1,012 | 215 | 3 | A |  |  |  |  |
|  |  | UT | 539 | 479 | 1,012 | 850 | 214 | F |  |  |  |  |
| Rte 7 at Potomac View Road | SB | RT | 563 | 194 | 759 | 1,300 | 99 | F | 99 | F | 31 | c |
|  | ев | LT | 54 | 353 | 1,099 | 480 | 69 | E | 36 | D |  |  |
|  |  | T | 3,054 | 353 | 1,099 | 910 | 36 | D |  |  |  |  |
|  |  | RT | 204 | 1 | 152 | 840 | 26 | c |  |  |  |  |
|  | NB | RT | 549 | 33 | 140 | 455 | 20 | B | 20 | B |  |  |
|  |  | LT | 347 | 189 | 691 | 420 | 114 | F | 27 | c |  |  |
|  | wB | T | 1,772 | 189 | 691 | 2,200 | 15 | B |  |  |  |  |
|  |  | RT | 371 | 3 | 149 | 330 | 6 | A |  |  |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping Center (Unsignalized) | wв | RT | 40 | 7 | 196 |  | 1 | A | 2 | A | 2 | A |
|  |  | T | 2,463 | 7 | 196 |  | 2 | A |  |  |  |  |
|  | SB | RT | 5 | 0 | 22 |  | 7 | A | 7 | A |  |  |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) | EB | RT | 16 | 466 | 976 |  | 33 | D | 54 | F | 56 | F |
|  |  | T | 3,501 | 466 | 976 |  | 54 | F |  |  |  |  |
|  | EB | $\stackrel{\text { RT }}{\text { UT }}$ | 178 | 92 | 257 | 1,250 | 452 | F | 452 | F | 52 | D |
| U-Turn - West of Sterling Blvd/Cardinal Glen Circle |  | T | 3,312 | 258 | 464 | 1,100 | 26 | c | 30 | c |  |  |
|  | wB | UT | 362 | 581 | 1,007 | 725 | 335 | F | 82 | F |  |  |
|  |  | T | 2,323 | 581 | 1,007 | 1,000 | 42 | D |  |  |  |  |
| Rte 7 at N Sterling Blvd/Cardinal Glen Circle | SB | RT | 65 | 48 | 216 | 405 | 109 | F | 109 | F | 42 | D |
|  | EB | LT | 3 | 462 | 974 | 580 | 86 | F | 40 | D |  |  |
|  |  | T | 3,408 | 462 | 974 | 2,180 | 42 | D |  |  |  |  |
|  |  | RT | 247 | 5 | 130 | 395 | 17 | B |  |  |  |  |
|  | NB | RT | 957 | 186 | 606 | 510 | 53 | D | 53 | D |  |  |
|  | wB | LT | 339 | 313 | 857 | 650 | 63 | E | 39 | D |  |  |
|  |  | T | 2,709 | 313 | 857 | 1,285 | 36 | D |  |  |  |  |
|  |  | RT | 18 | 0 | 0 | 305 | 8 | A |  |  |  |  |
| U-Turn - West of Augusta Dr | EB | UT | 382 | 335 | 914 | 700 | 134 | F | 26 | D | 24 | c |
|  |  | T | 3,937 | 335 | 914 | 800 | 16 | B |  |  |  |  |
|  |  | T | 2,741 | 204 | 597 | 400 | 21 | c | 21 | c |  |  |
| Rte 7 at Augusta Dr | SB | RT | 621 | 131 | 496 | 205 | 80 | E | 80 | в | 26 |  |
|  |  | LT | 131 | 165 | 562 | 6220 | 97 | F | 14 |  |  |  |
|  |  | T | 3,803 | 165 | 562 | $\frac{1,300}{}$ | 11 | B |  |  |  | c |
|  | wB | T | 2,153 | 188 | 723 | 790 | ${ }^{110}$ | c | 32 | c |  |  |
|  |  | RT | 157 | 3 | 101 | 400 | 13 | B |  |  |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | EB | RT | 40 | 66 | 465 |  |  | A | 9 | A | 9 | A |
|  |  | ${ }^{\text {T }}$ | 3,770 | 66 | 465 |  | 9 | A |  |  |  |  |
| Rte 7 at Cedar Dr | NB | RT | 5 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  | SB | RT | 33 | 6 | 63 | 220 | 35 | c | 35 |  | 18 | B |
|  | EB | LT | 69 | 158 | 457 | 550 | 102 | F | 16 | B |  |  |
|  |  | T | 3,697 | 158 | 457 | 800 | 14 | B |  |  |  |  |
|  |  | RT | 5 | 158 | 457 | 335 | 1 | A |  |  |  |  |
|  | NB | RT | 104 | 23 | 121 | 100 | 56 | E | 56 | E |  |  |
|  | wB | T | 2,334 | 116 | 445 | 880 | 12 | B | 19 | B |  |  |
|  |  | RT | 22 | 116 | 445 | 450 | 1 | A |  |  |  |  |
|  |  | UT | 142 | 116 | 445 | 800 | 136 | F |  |  |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | RT1 | 19 | 60 | 326 |  | 9 | A | 9 |  | 9 | A |
|  |  | RT2 | 111 | 0 | 0 |  | 4 | A |  | A |  |  |
|  |  | T | 3,927 | 60 | 326 |  | 9 | A |  |  |  |  |
|  | NB | RT | 0 | 0 | 0 |  | 0 | A | 0 | A |  |  |
|  | WB | ${ }_{\text {RT }}$ | 10 | 21 | 178 |  | 1 | A | 4 | A |  |  |
| (Unsignalized) | SB | $\stackrel{\text { T }}{\text { RT }}$ | $\frac{2,508}{8}$ | 21 | 178 0 |  | 4 | A | ${ }_{0}$ | A | 4 | A |

Travel Time: Rte 7 Between Rte 28 and Dranesville Rd

|  | Model Travel Time (min) |
| :--- | :---: |
| Eastbound | 11.3 |
| Westbound | 8.6 |



| Intersection /Interchange | Movement | Speed | Volume (vph) | Density (vpmpl) | Los |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Junction | 46 | 2,677 | 14 | B |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 47 | 2,349 | 17 | B |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 45 | 2,718 | 15 | B |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 54 | 3,702 | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Junction | 52 | 3,476 | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 44 | 3,052 | 23 | B |
|  | Rte 7 at Atlantic Blvd EB On-ramp Junction | 31 | 3,497 | 28 | D |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Junction | 42 | 2,026 | 12 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment | 43 | 1,683 | 13 | B |
|  | Rte 7 at Cascades Pkwy WB On-ramp Junction | 24 | 2,001 | 21 | C |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Junction | 25 | 3,031 | 30 | D |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment | 19 | 2,503 | 43 | E |
|  | Rte 7 at Cascades Pkwy EB On-ramp Junction | 10 | 2,793 | 73 | E |


Travel Time: Rte 7 Between Rte 28 and Dranesville Rd

|  | Model Travel Time (min) |
| :---: | :---: |
| Eastbound | 7.8 |
| Westbound | 11.0 |



| Intersection /Interchange | Movement | Speed | Volume (vph) | Density (vpmpl) | Los |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Junction | 45 | 3,631 | 20 | c |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 46 | 3,189 | 23 | c |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 44 | 3,916 | 22 | C |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 54 | 3,637 | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Junction | 53 | 3,410 | 16 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 48 | 2,527 | 18 | C |
|  | Rte 7 at Atlantic Blvd EB On-ramp Junction | 39 | 3,042 | 20 | B |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Junction | 39 | 2,964 | 19 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment | 43 | 2,495 | 19 | c |
|  | Rte 7 at Cascades Pkwy WB On-ramp Junction | 21 | 3,275 | 40 | E |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Junction | 33 | 3,057 | 23 | c |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment | 47 | 2,047 | 15 | B |
|  | Rte 7 at Cascades Pkwy EB On-ramp Junction | 21 | 2,591 | 30 | D |

## Appendix H:

## Comparison of VISSIM Results 2040 Build Alternative 1 Conditions vs.

 2040 No-Build ConditionsLC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Intersecton Delay and LOS, AM Peak Hour

| Intersection | 2040 No-Build |  |  |  |  | 2040 Alternative 1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach Direction | Approach Delay (sec/veh) | Approach LOS | Intersection Delay (sec/veh) | Intersection LOS | Approach Delay (sec/veh) | $\begin{gathered} \text { Approach } \\ \text { LOS } \end{gathered}$ | Intersection Delay (sec/veh) | Intersection LOS |
| Rte 7 at Broad Run Drive (Unsignalized) | WB | 0 | A | 0 | A | 1 | A | 1 | A |
|  | SB | 9 | A |  |  | 10 | A |  |  |
| Jona Driveway (Unsignalized) | WB | 0 | A | 0 | A | 1 | A | 1 | A |
| Rte 7 at City Center Blvd/Countryside Blvd | SB | 50 | D | 23 | C | 64 | E | 27 | C |
|  | EB | 22 | c |  |  | 25 | c |  |  |
|  | NB | 58 | E |  |  | 87 | F |  |  |
|  | WB | 15 | B |  |  | 20 | B |  |  |
| Rte 7 at Davenport Drive <br> (Unsignalized under No-Build; Signalized under Alternative 1) | WB | 1 | A | 2 | A | 21 | C | 33 | C |
|  | SB | 14 | B |  |  | 111 | F |  |  |
|  | EB | N/A | N/A |  |  | 39 | D |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | 27 | C | 23 | C | 69 | E | 22 | C |
|  | EB | 24 | C |  |  | 18 | B |  |  |
|  | NB | 55 | D |  |  | 68 | E |  |  |
|  | WB | 16 | B |  |  | 24 | C |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | 103 | F | 34 | C | 10 | A | 80 | E |
|  | EB | 55 | D |  |  | 85 | F |  |  |
|  | NB | 24 | C |  |  | 393 | F |  |  |
|  | WB | 10 | A |  |  | 50 | D |  |  |
| Rte 7 at Potomac View Road | SB | 74 | E | 51 | D | 99 | F | 31 | C |
|  | EB | 27 | C |  |  | 36 | D |  |  |
|  | NB | 171 | F |  |  | 20 | B |  |  |
|  | WB | 47 | D |  |  | 27 | C |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping Center (Unsignalized) | WB | 6 | A | 6 | A | 2 | A | 2 | A |
|  | SB | 19 | C |  |  | 7 | A |  |  |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) | EB | 27 | D | 29 | D | 54 | F | 56 | F |
|  | NB | 358 | F |  |  | 452 | F |  |  |
| U-Turn - West of Sterling Blvd/Cardinal Glen Circle <br> (Does not exist for No-Build) | EB | N/A | N/A | N/A | N/A | 30 | C | 52 | D |
|  | WB | N/A | N/A |  |  | 82 | F |  |  |

LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Intersecton Delay and LOS, AM Peak Hour

| Intersection | 2040 No-Build |  |  |  |  | 2040 Alternative 1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach Direction | Approach Delay (sec/veh) | Approach LOS | $\begin{array}{c}\text { Intersection Delay } \\ \text { (sec/veh) }\end{array}$ | $\begin{gathered} \text { Intersection } \\ \text { LOS } \end{gathered}$ | Approach Delay (sec/veh) | Approach LOS | Intersection Delay (sec/veh) | $\begin{aligned} & \text { Intersection } \\ & \text { LOS } \end{aligned}$ |
| Rte 7 at N Sterling Blvd/Cardinal Glen Circle | SB | 70 | E | 29 | C | 109 | F | 42 | D |
|  | EB | 23 | c |  |  | 40 | D |  |  |
|  | NB | 46 | D |  |  | 53 | D |  |  |
|  | WB | 29 | C |  |  | 39 | D |  |  |
| U-Turn - West of August Dr | EB | N/A | N/A | N/A | N/A | 26 | D | 24 | C |
| (Does not exist for No-Build) | WB |  |  |  |  | 21 | C |  |  |
| Rte 7 at Augusta Dr | SB | 62 | E | 23 | C | 80 | E | 26 | C |
|  | EB | 24 | c |  |  | 14 | B |  |  |
|  | WB | 11 | B |  |  | 32 | c |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | EB | 19 | c | 19 | C | 9 | A | 9 | A |
|  | NB | 118 | F |  |  | 0 | A |  |  |
| Rte 7 at Cedar Dr <br> (Unsignalized for No-Build; Signalized for Alternative 1) | SB | 81 | F | 13 | B | 35 | c | 18 | B |
|  | EB | 19 | c |  |  | 16 | B |  |  |
|  | NB | 52 | F |  |  | 56 | E |  |  |
|  | WB | 1 | A |  |  | 19 | B |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | 15 | B | 15 | B | 9 | A | 9 | A |
|  | NB | 271 | F |  |  | 0 | A |  |  |
| Rte 7 at Driveway to Cedar Lake Plaza (Unsignalized) | WB | 0 | A | 0 | A | 4 | A | 4 | A |
|  | SB | 0 | A |  |  | 0 | A |  |  |
| Rte 7 at Community Plaza/Lakeland Drive | SB | 81 | F | 13 | B | 92 | F | 16 | B |
|  | EB | 12 | B |  |  | 9 | A |  |  |
|  | NB | 44 | D |  |  | 2 | A |  |  |
|  | WB | 5 | A |  |  | 19 | B |  |  |
| Rte 7 at NB Driveways between Community Plaza and Dranesville Road (Unsignalized) | EB | 1 | A | 1 | A | 3 | A | 3 | A |
|  | NB | 1 | A |  |  | 2 | A |  |  |

LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Intersecton Delay and LOS, AM Peak Hour


LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Intesection Delay and LOS, PM Peak Hour

| Intersection | 2040 No-Build |  |  |  |  | 2040 Alternative 1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach Direction | Approach Delay (sec/veh) | $\begin{aligned} & \text { Approach } \\ & \text { LOS } \end{aligned}$ | Intersection Delay (sec/veh) | Intersection LOS | Approach Delay (sec/veh) | $\begin{aligned} & \text { Approach } \\ & \text { LOS } \end{aligned}$ | Intersection Delay (sec/veh) | Intersection LOS |
| Rte 7 at Broad Run Drive (Unsignalized) | WB | 2 | A | 2 | A | 3 | A | 3 | A |
|  | SB | 24 | C |  |  | 24 | C |  |  |
| Jona Driveway (Unsignalized) | WB | 0 | A | 0 | A | 0 | A | 0 | A |
| Rte 7 at City Center Blvd/Countryside Blvd | SB | 61 | E | 31 | C | 34 | C | 33 | C |
|  | EB | 29 | C |  |  | 28 | C |  |  |
|  | NB | 45 | D |  |  | 70 | E |  |  |
|  | WB | 25 | C |  |  | 32 | C |  |  |
| Rte 7 at Davenport Drive <br> (Unsignalized under No-Build; Signalized under Alternative 1) | WB | 2 | A | 3 | A | 6 | A | 19 | B |
|  | SB | 23 | C |  |  | 110 | F |  |  |
|  | EB | N/A | N/A |  |  | 13 | B |  |  |
| Rte 7 at Loudoun Tech Dr/Palisades Pkwy | SB | 37 | D | 41 | D | 21 | C | 20 | B |
|  | EB | 57 | E |  |  | 16 | B |  |  |
|  | NB | 60 | E |  |  | 18 | B |  |  |
|  | WB | 21 | C |  |  | 23 | C |  |  |
| Rte 7 at Bartholomew Fair Dr/Campus Dr | SB | 94 | F | 19 | B | 16 | B | 32 | C |
|  | EB | 18 | B |  |  | 38 | D |  |  |
|  | NB | 42 | D |  |  | 86 | F |  |  |
|  | WB | 13 | B |  |  | 17 | B |  |  |
| Rte 7 at Potomac View Road | SB | 82 | F | 41 | D | 63 | E | 31 | C |
|  | EB | 27 | C |  |  | 28 | C |  |  |
|  | NB | 65 | E |  |  | 15 | B |  |  |
|  | WB | 35 | C |  |  | 31 | C |  |  |
| Rte 7 at Driveway to Mirror Ridge Shopping Center (Unsignalized) | WB | 14 | B | 15 | C | 5 | A | 5 | A |
|  | SB | 159 | F |  |  | 70 | F |  |  |
| Rte 7 at Driveway to Cascades Village Residential Development and Rehabilitation Center (Unsignalized) | EB | 2 17 | A | 2 | A | 9 39 | E | 9 | A |
| U-Turn - West of Sterling Blvd/Cardinal Glen Circle <br> (Does not exist for No-Build) | EB | N/A | N/A | N/A | N/A | 11 | B | 14 | B |
|  | WB | N/A | N/A |  |  | 18 | B |  |  |

LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Intesection Delay and LOS, PM Peak Hour

| Intersection | 2040 No-Build |  |  |  |  | 2040 Alternative 1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach Direction | Approach Delay (sec/veh) | Approach LOS | Intersection Delay (sec/veh) | Intersection LOS | Approach Delay (sec/veh) | $\begin{gathered} \text { Approach } \\ \text { LOS } \end{gathered}$ | Intersection Delay (sec/veh) | $\qquad$ |
| Rte 7 at N Sterling Blvd/Cardinal Glen Circle | SB | 71 | E | 33 | C | 21 | C | 11 | B |
|  | EB | 27 | C |  |  | 8 | A |  |  |
|  | NB | 48 | D |  |  | 27 | C |  |  |
|  | WB | 32 | C |  |  | 9 | A |  |  |
| U-Turn - West of August Dr | EB | N/A | N/A | N/A | N/A | 12 | B | 11 | B |
| (Does not exist for No-Build) | WB |  |  |  |  | 10 | A |  |  |
| Rte 7 at Augusta Dr | SB | 61 | E | 18 | B | 50 | D | 28 | C |
|  | EB | 10 | A |  |  | 10 | A |  |  |
|  | WB | 20 | B |  |  | 47 | D |  |  |
| Rte 7 at Driveway to Christ the Redeemer Catholic Church (Unsignalized) | EB | 1 | A | 1 | A | 1 | A | 1 | A |
|  | NB | 9 | A |  |  | 0 | A |  |  |
| Rte 7 at Cedar Dr <br> (Unsignalized for No-Build; Signalized for Alternative 1) | SB | 166 | F | 11 | B | 81 | F | 35 | C |
|  | EB | 3 | A |  |  | 14 | B |  |  |
|  | NB | 60 | F |  |  | 314 | F |  |  |
|  | WB | 15 | B |  |  | 29 | C |  |  |
| Rte 7 at Driveway to Chick-fil-A (Unsignalized) | EB | 4 | A | 5 | A | 2 | A | 2 | A |
|  | NB | 62 | F |  |  | 10 | A |  |  |
| Rte 7 at Driveway to Cedar Lake Plaza (Unsignalized) | WB | 8 | A | 8 | A | 18 | C | 18 | C |
|  | SB | 1 | A |  |  | 0 | A |  |  |
| Rte 7 at Community Plaza/Lakeland Drive | SB | 65 | E | 20 | B | 75 | E | 69 | E |
|  | EB | 20 | B |  |  | 13 | B |  |  |
|  | NB | 62 | E |  |  | 2 | A |  |  |
|  | WB | 7 | A |  |  | 143 | F |  |  |
| Rte 7 at NB Driveways between Community Plaza and Dranesville Road (Unsignalized) | EB | 1 | A | 1 | A | 1 | A | 1 | A |
|  | NB | 3 | A |  |  | 2 | A |  |  |

LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Intesection Delay and LOS, PM Peak Hour


LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Interchange Density and LOS, AM Peak Hour

| Interchange | Location | 2040 No-Build |  | 2040 Alternative 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Density (vpmpl) | LOS | Density (vpmpl) | LOS |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Diverge | 13 | B | 14 | B |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 17 | B | 17 | B |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 15 | B | 15 | B |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 17 | B | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Diverge | 16 | B | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 21 | B | 23 | B |
|  | Rte 7 at Atlantic Blvd EB On-ramp Merge | 30 | D | 28 | D |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Diverge | 13 | B | 12 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment (Weaving segment for No-Build) | 12 | B | 13 | B |
|  | Rte 7 at Cascades Pkwy WB On-ramp Merge | 17 | B | 21 | C |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Diverge | 82 | E | 30 | D |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment (Wevaing segment for No-Build) | 97 | F | 43 | E |
|  | Rte 7 at Cascades Pkwy EB On-ramp Merge | 113 | E | 73 | E |

LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Interchange Density and LOS, PM Peak Hour

| Interchange | Location | 2040 No-Build |  | 2040 Alternative 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Density (vpmpl) | LOS | Density (vpmpl) | LOS |
| Rte 7 at Atlantic Blvd Interchange | Rte 7 at Atlantic Blvd WB Off-ramp Diverge | 18 | B | 20 | C |
|  | Rte 7 at Atlantic Blvd WB Basic Freeway Segment | 22 | C | 23 | C |
|  | Rte 7 at Atlantic Blvd WB Weaving Segment | 22 | C | 22 | C |
|  | Rte 7 at Atlantic Blvd EB Weaving Segment | 17 | B | 17 | B |
|  | Rte 7 at Atlantic Blvd EB Off-ramp Diverge | 16 | B | 16 | B |
|  | Rte 7 at Atlantic Blvd EB Basic Freeway Segment | 18 | C | 18 | C |
|  | Rte 7 at Atlantic Blvd EB On-ramp Merge | 19 | B | 20 | B |
| Rte 7 at Cascades Pkwy Interchange | Rte 7 at Cascades Pkwy WB Off-ramp Diverge | 18 | B | 19 | B |
|  | Rte 7 at Cascades Pkwy WB Basic Freeway Segment (Weaving segment for No-Build) | 21 | C | 19 | C |
|  | Rte 7 at Cascades Pkwy WB On-ramp Merge | 44 | E | 40 | E |
|  | Rte 7 at Cascades Pkwy EB Off-ramp Diverge | 15 | B | 23 | C |
|  | Rte 7 at Cascades Pkwy EB Basic Freeway Segment (Wevaing segment for No-Build) | 17 | B | 15 | B |
|  | Rte 7 at Cascades Pkwy EB On-ramp Merge | 17 | B | 30 | D |

## LC_Rte 7_VISSIM Results: Comparison of 2040 Alternative 1 vs. 2040 No-Build Average Travel Times

Route 7 Between Route 28 and Dranesville Rd

| Direction | AM Peak Hour <br> Modeled Travel Time <br> (minutes) |  | PM Peak Hour <br> Modeled Travel Time <br> (minutes) |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{2 0 4 0}$ <br> No-Build | $\mathbf{2 0 4 0}$ <br> Alternative 1 | $\mathbf{2 0 4 0}$ <br> No-Build | $\mathbf{2 0 4 0}$ <br> Alternative 1 |
| Eastbound | 15.6 | 11.3 | 9.4 | 7.8 |
| Westbound | 7.2 | 8.6 | 10.7 | 11.0 |

